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(54) **MOBILE COILED TUBING REEL UNIT, RIG AND ARRANGEMENTS THEREOF**

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**E21B 19/00** (2006.01)  
**E21B 7/02** (2006.01)

(52) **U.S. Cl.**  
CPC ..... **E21B 19/22** (2013.01); **E21B 7/02** (2013.01); **E21B 7/023** (2013.01); **E21B 19/00** (2013.01)

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**E21B 7/026**; **E21B 19/22**  
See application file for complete search history.

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*Primary Examiner* — David Andrews

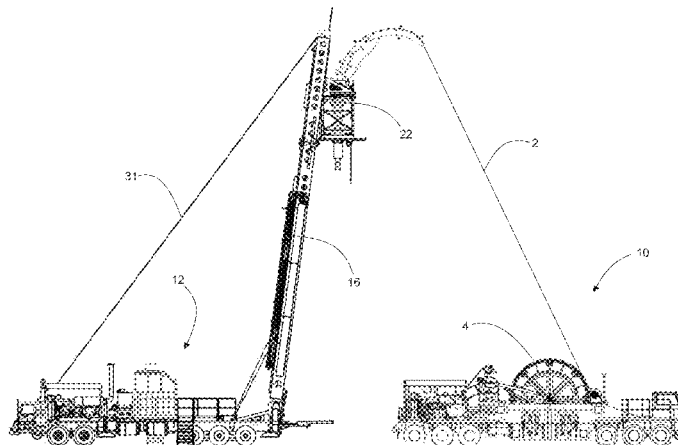
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(57) **ABSTRACT**

A system is provided for injecting coiled tubing (CT) into and out of a wellbore. In embodiments, separate injector and reel units are provided releasing constraints on CT size and length. The injector unit is fit with an extendible mast for handling larger bottom hole assemblies and fit with a rotating gooseneck for accepting CT from alternate arrangements of the reel unit. The mast is reinforced to resist CT loading. The capacity of the reel is maximized for the reel unit transport envelope. The reel is rotated using an offset drive engaging a bounding reel flange, such as engaging drive and bull gears. A generally radial displacement of the drive from the reel permits replacement of the entire reel.

**8 Claims, 22 Drawing Sheets**



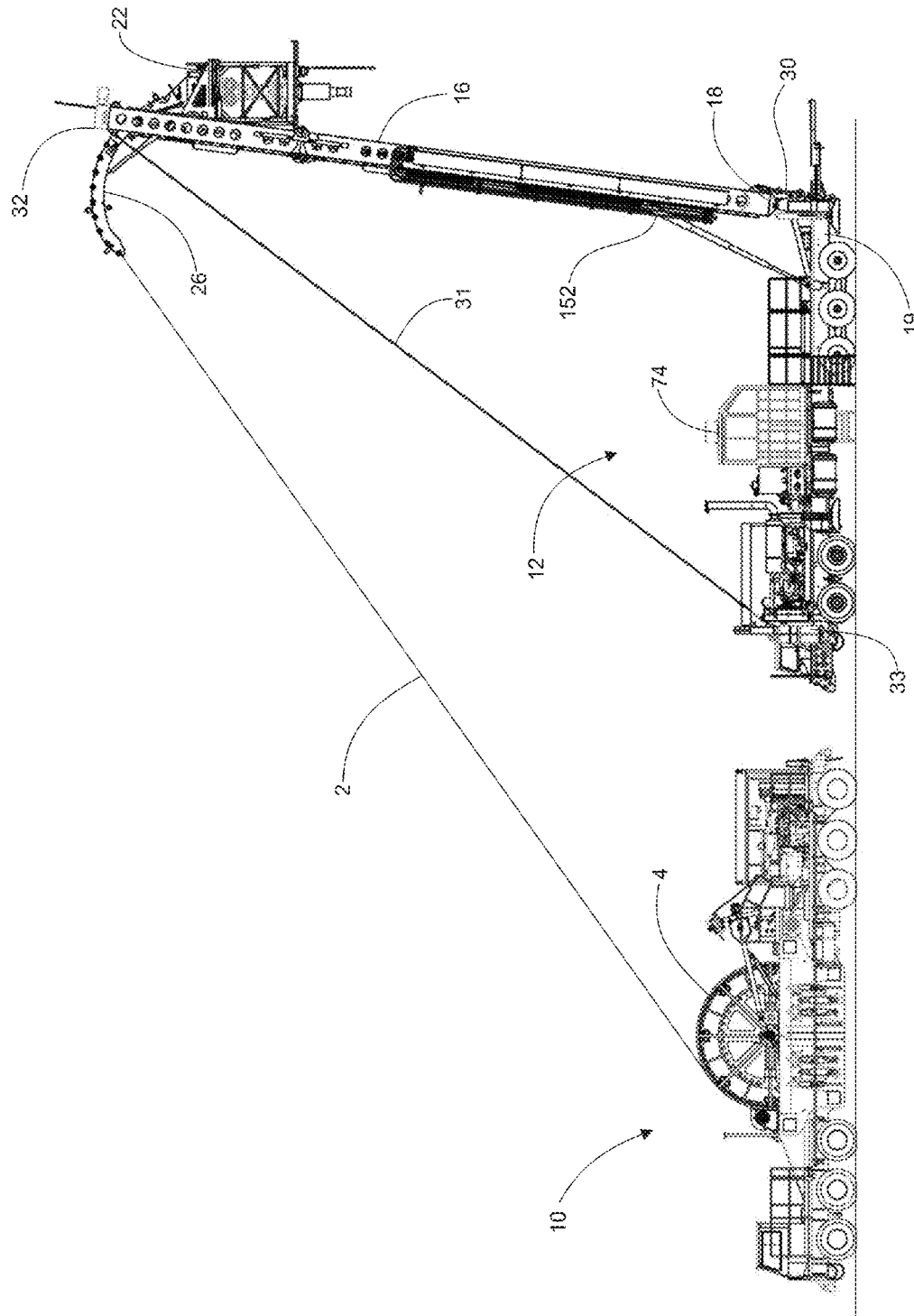


Fig. 1A

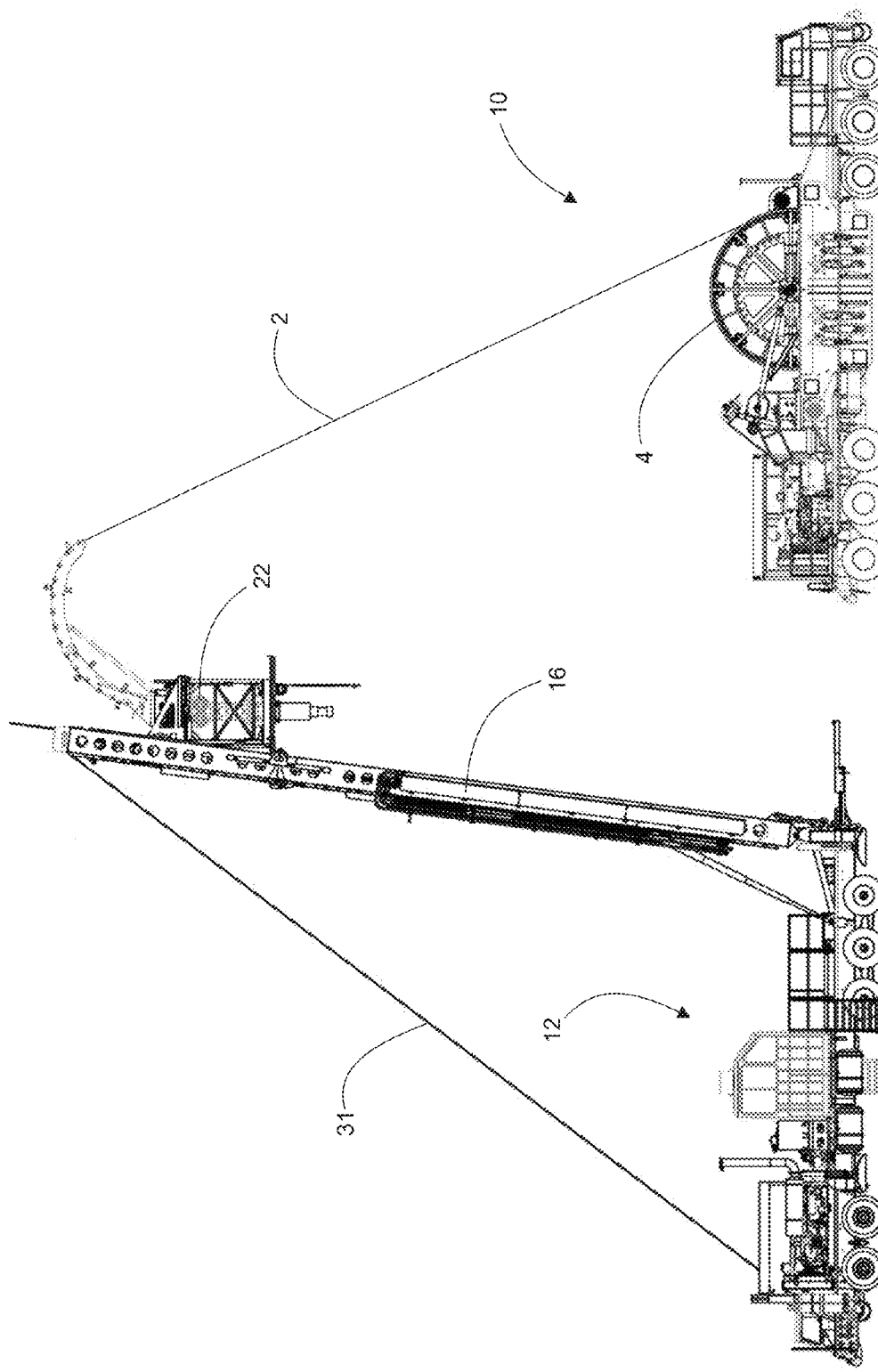
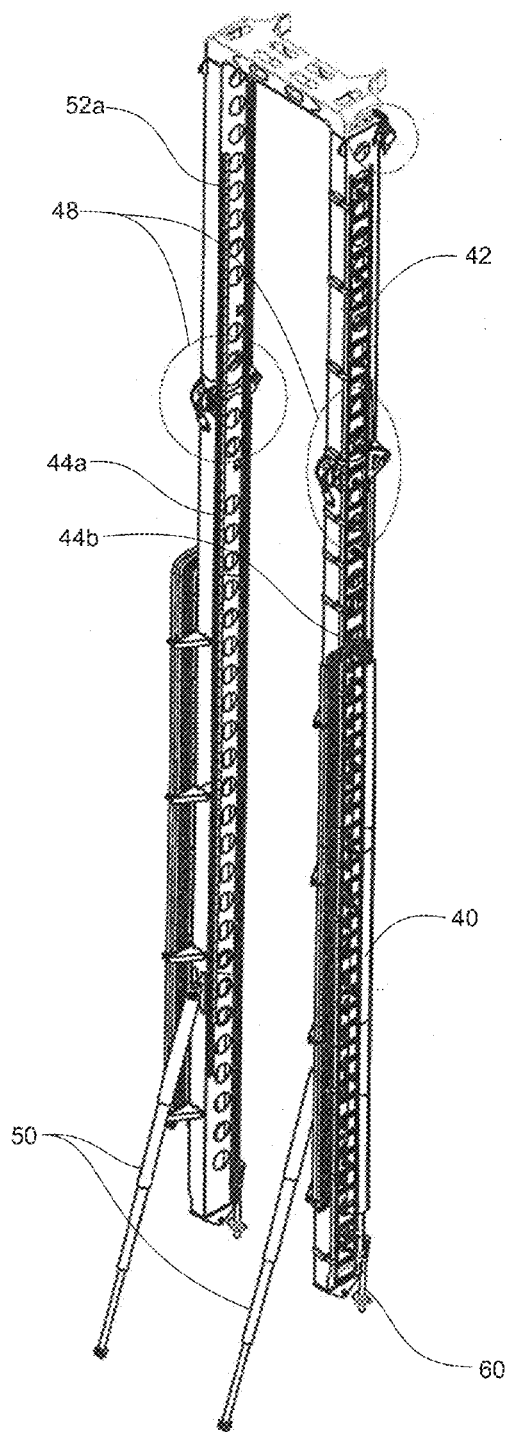
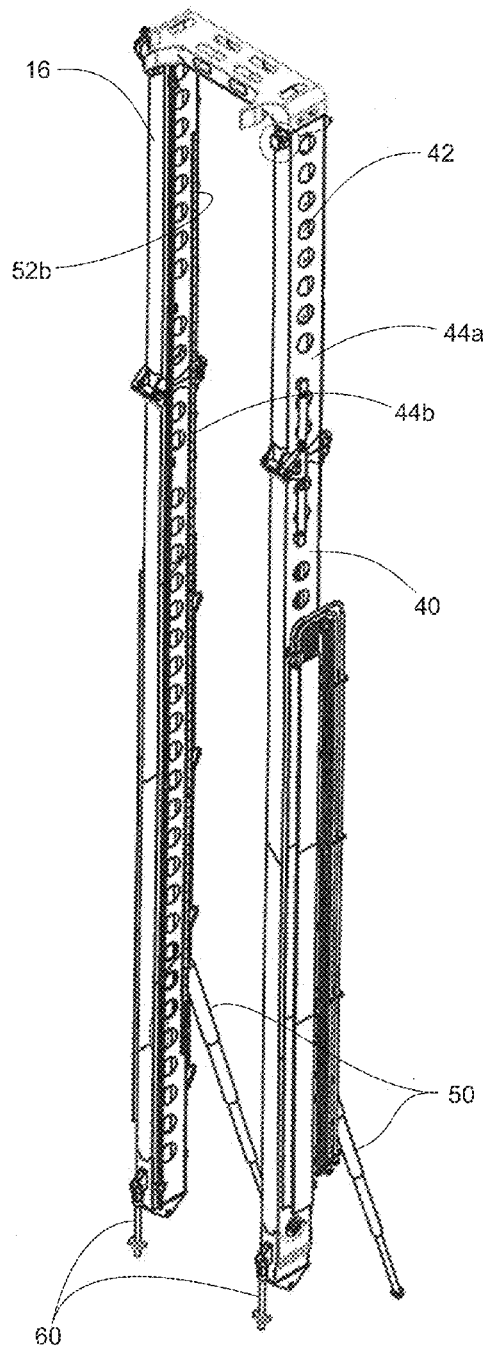


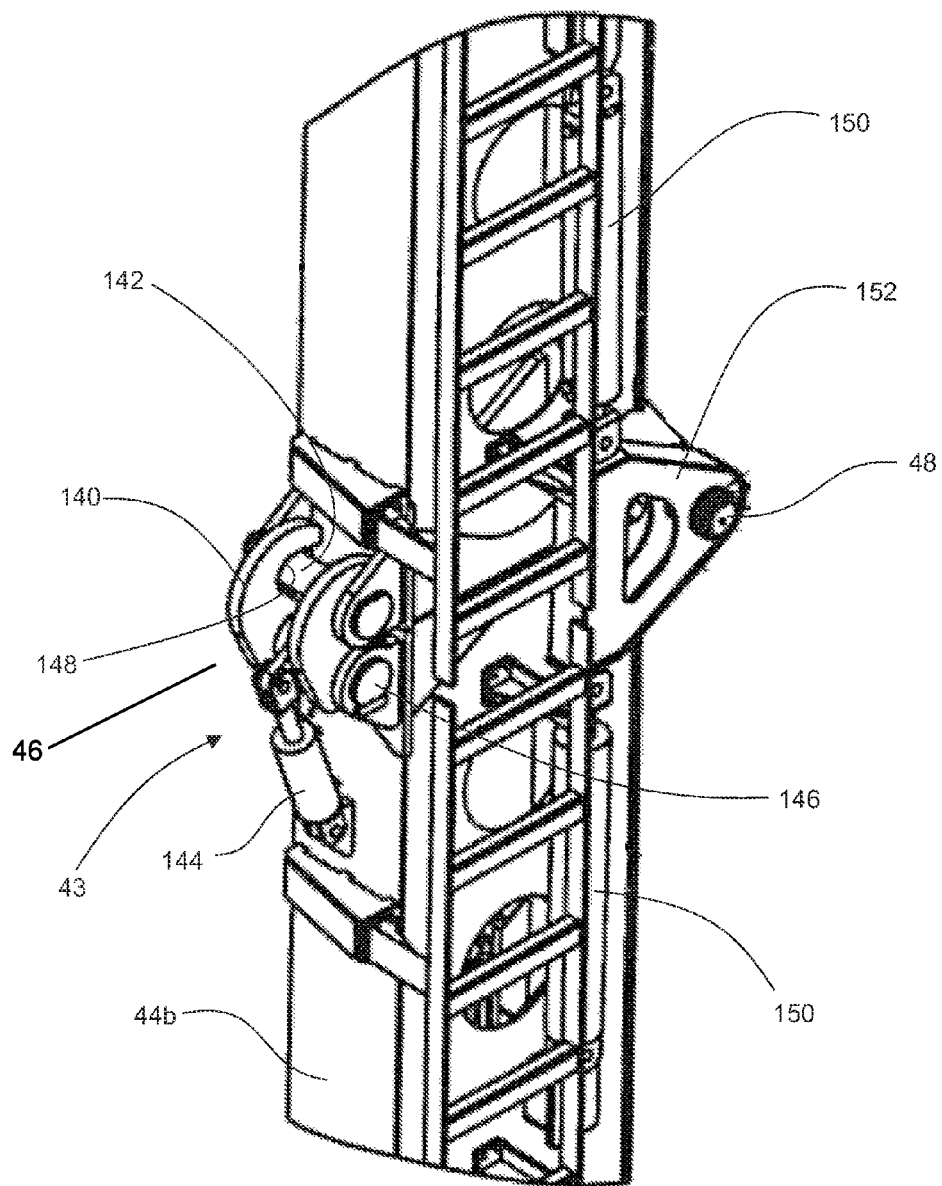
Fig. 1B



**Fig. 2A**



**Fig. 2B**



**Fig. 2C**

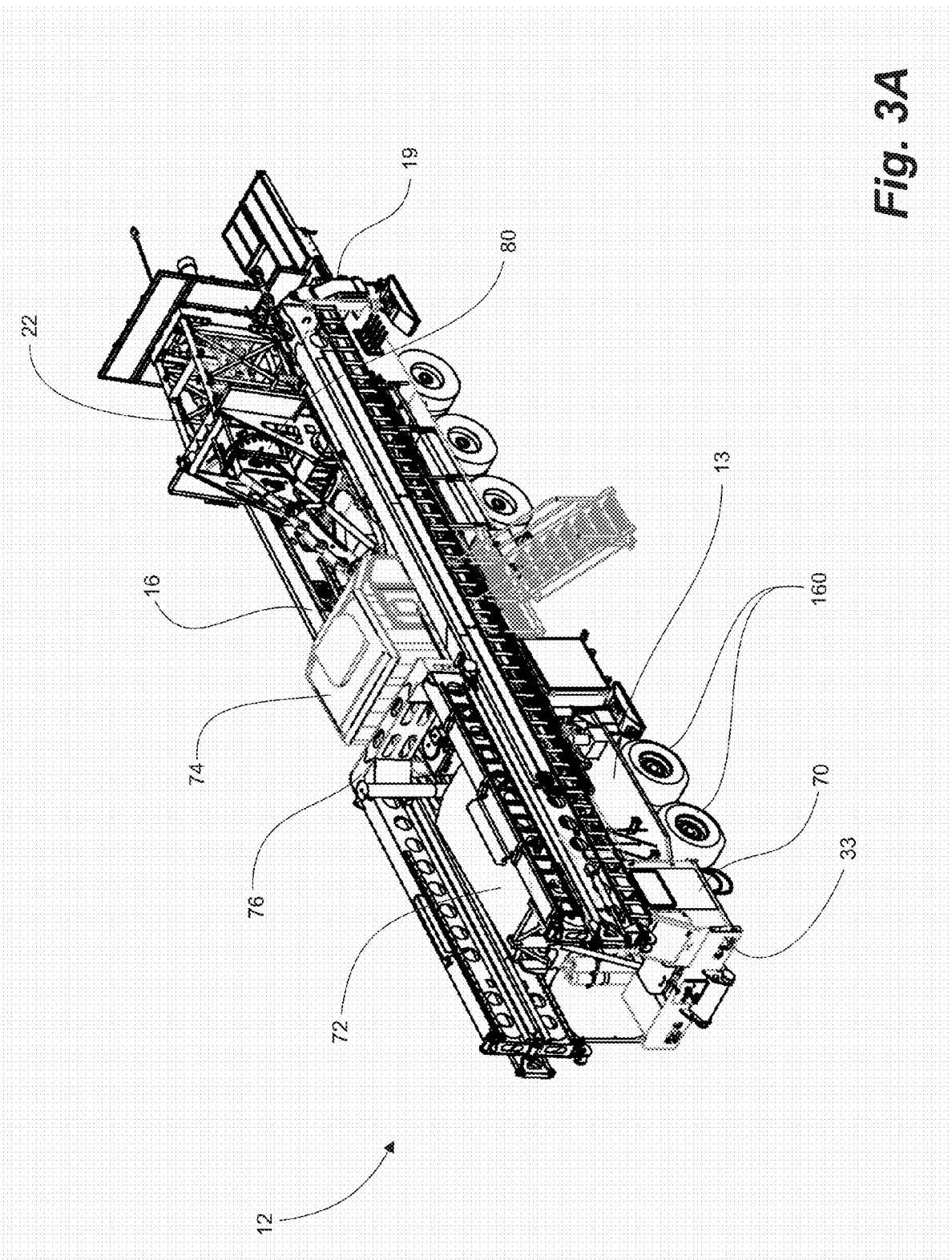
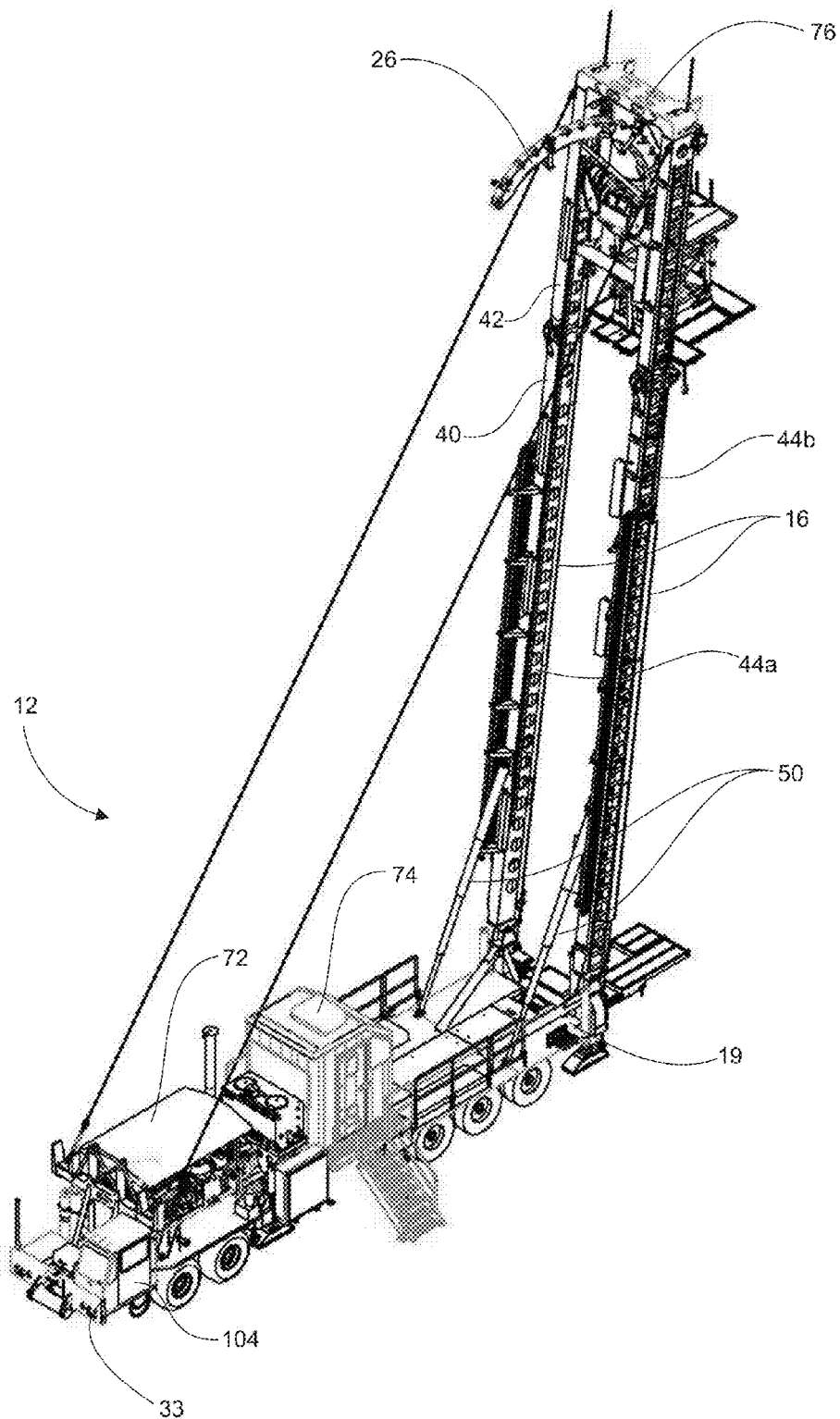
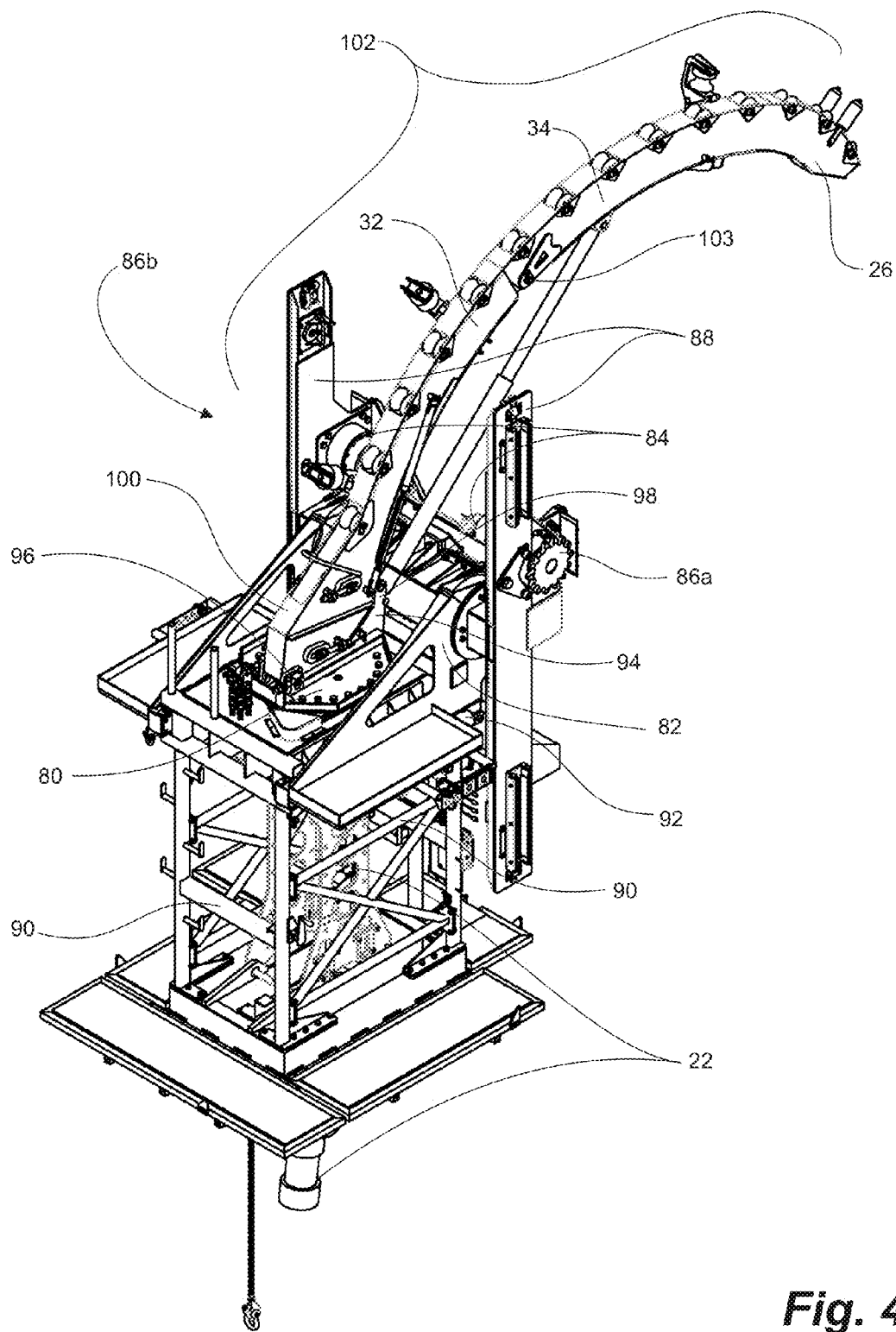


Fig. 3A

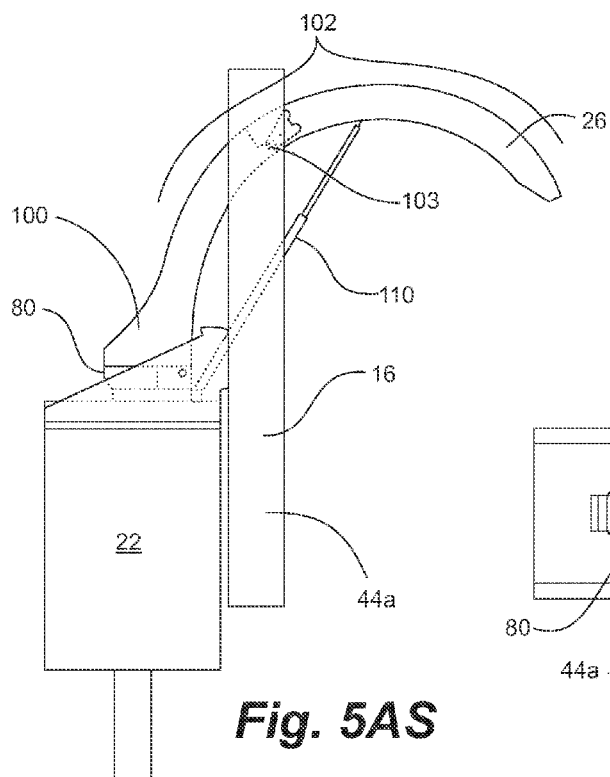


**Fig. 3B**

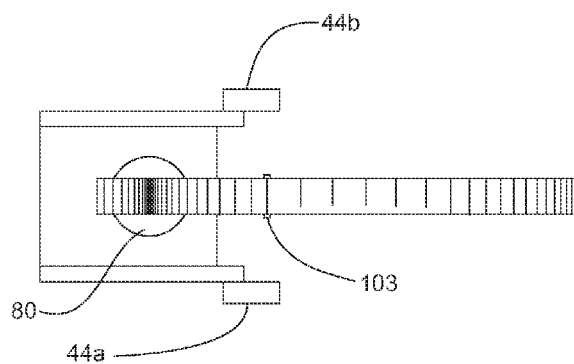


**Fig. 4**

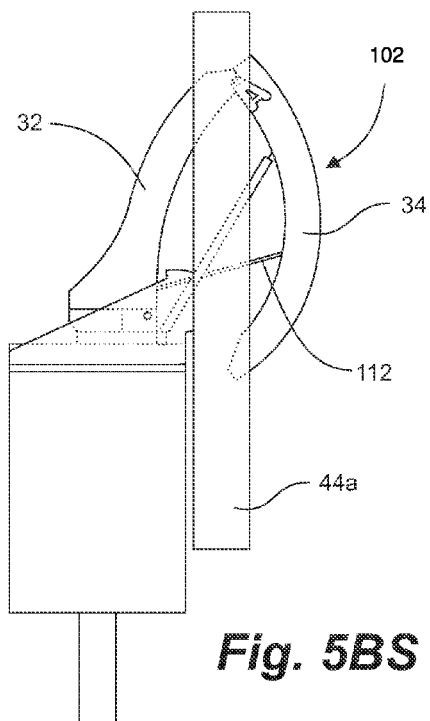




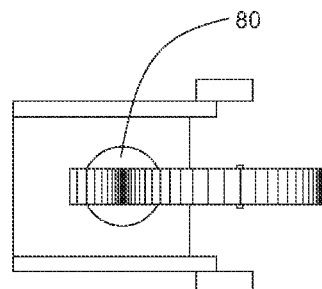
**Fig. 5AS**



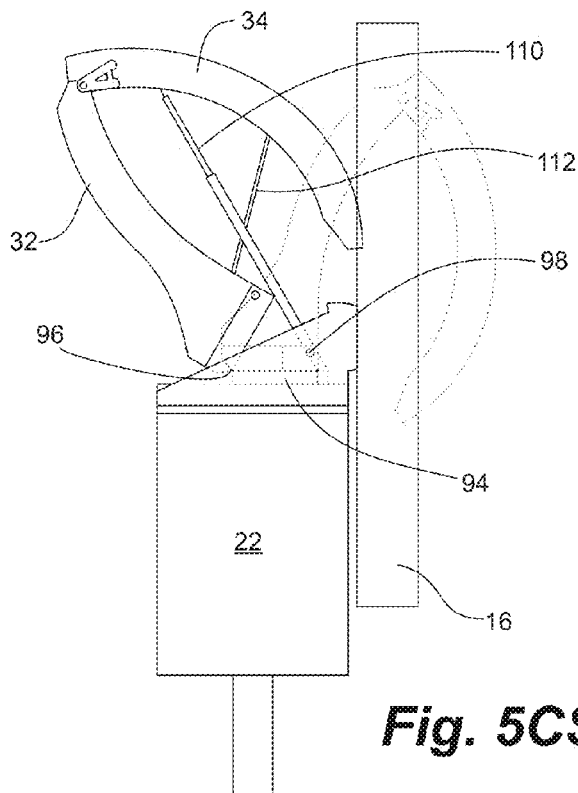
**Fig. 5AT**



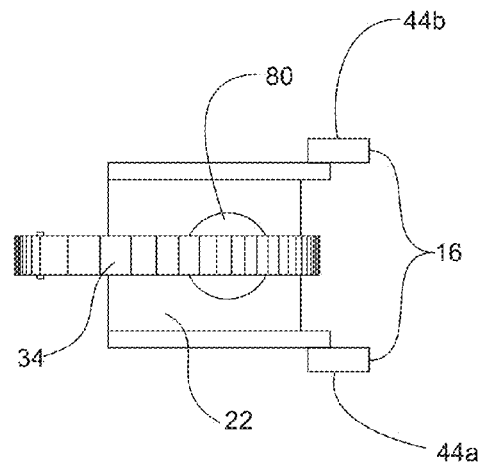
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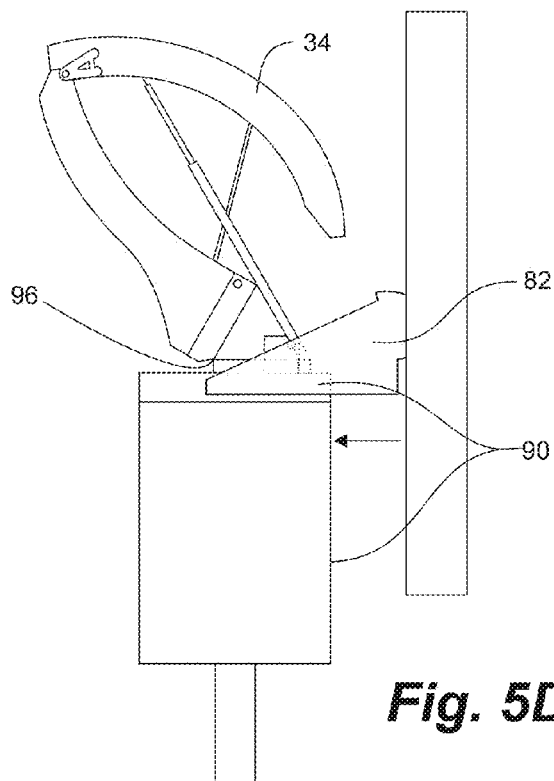
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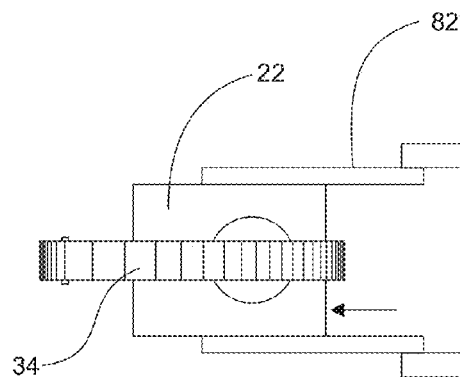
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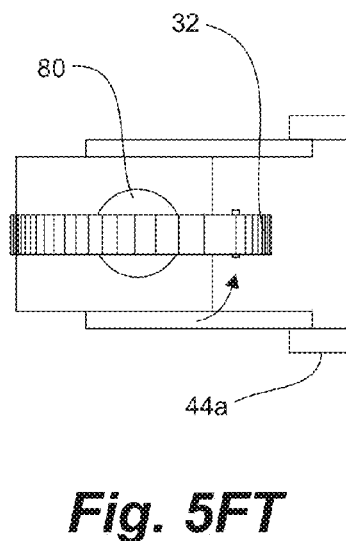
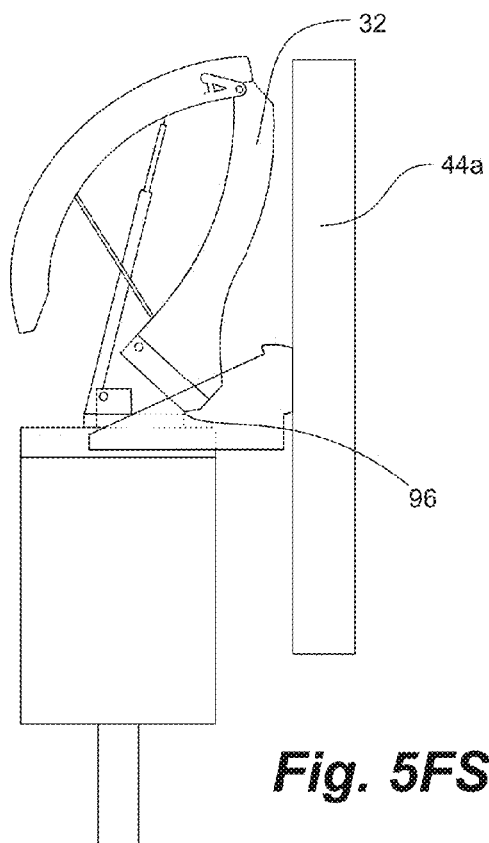
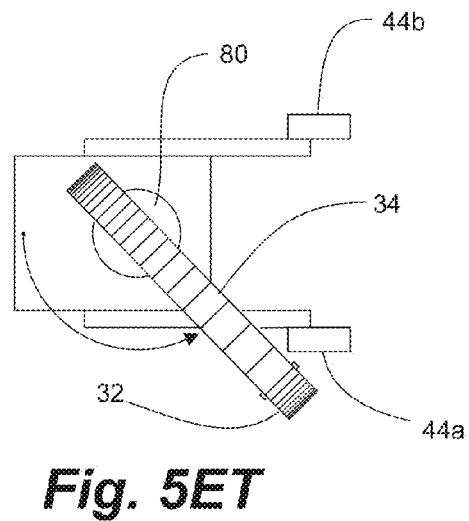
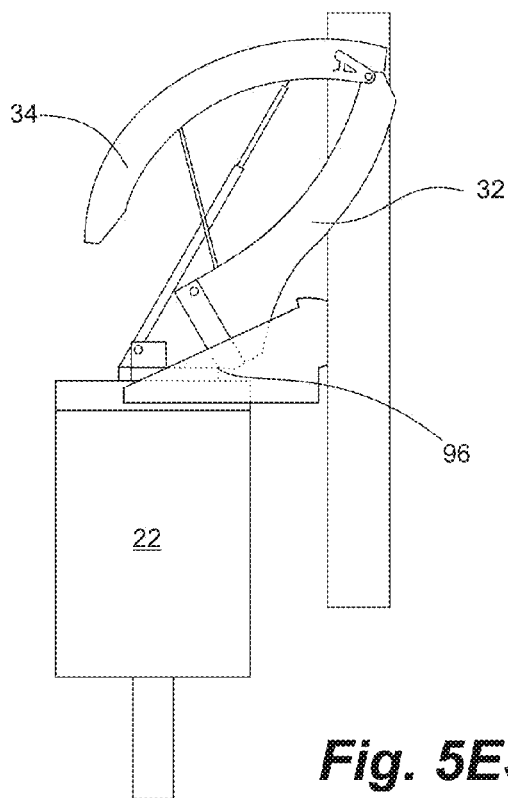
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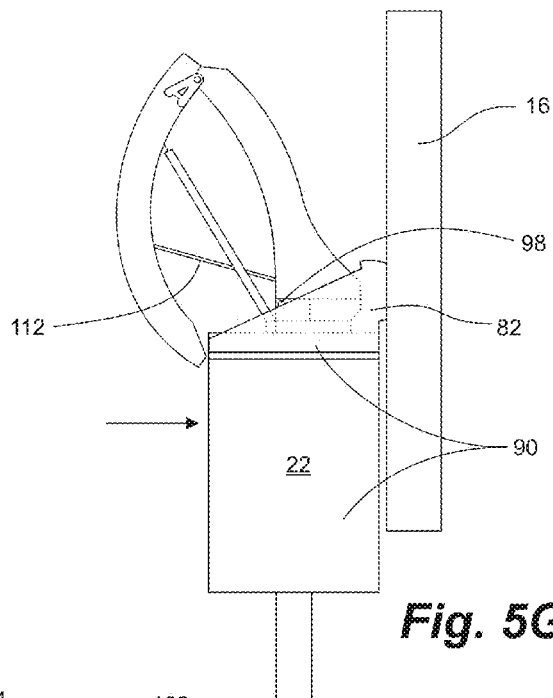


**Fig. 5DS**

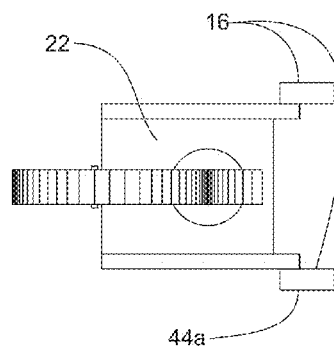


**Fig. 5DT**

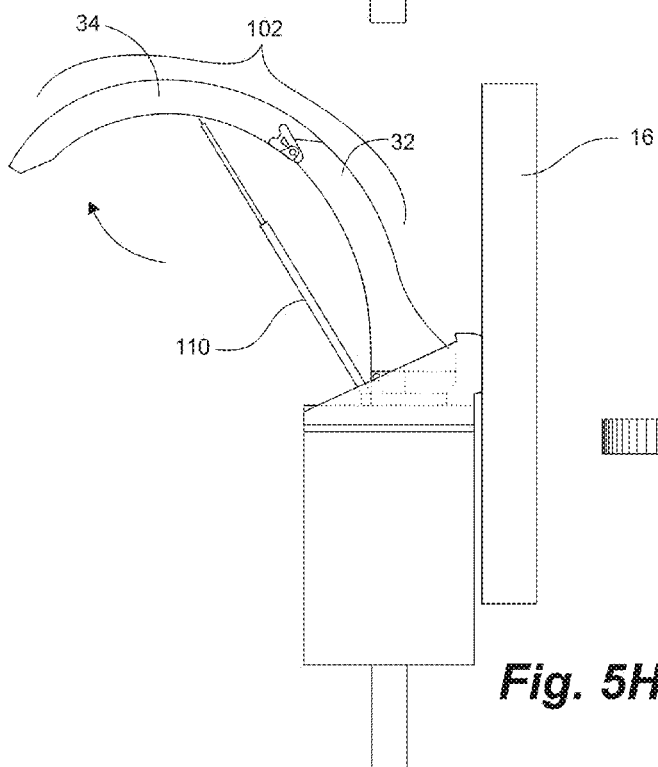




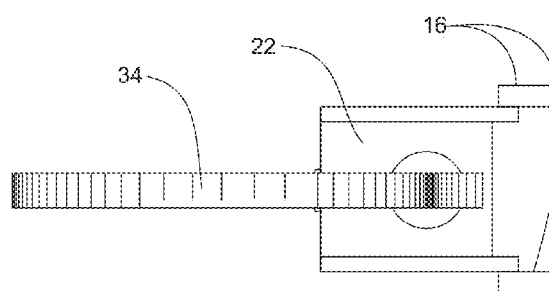
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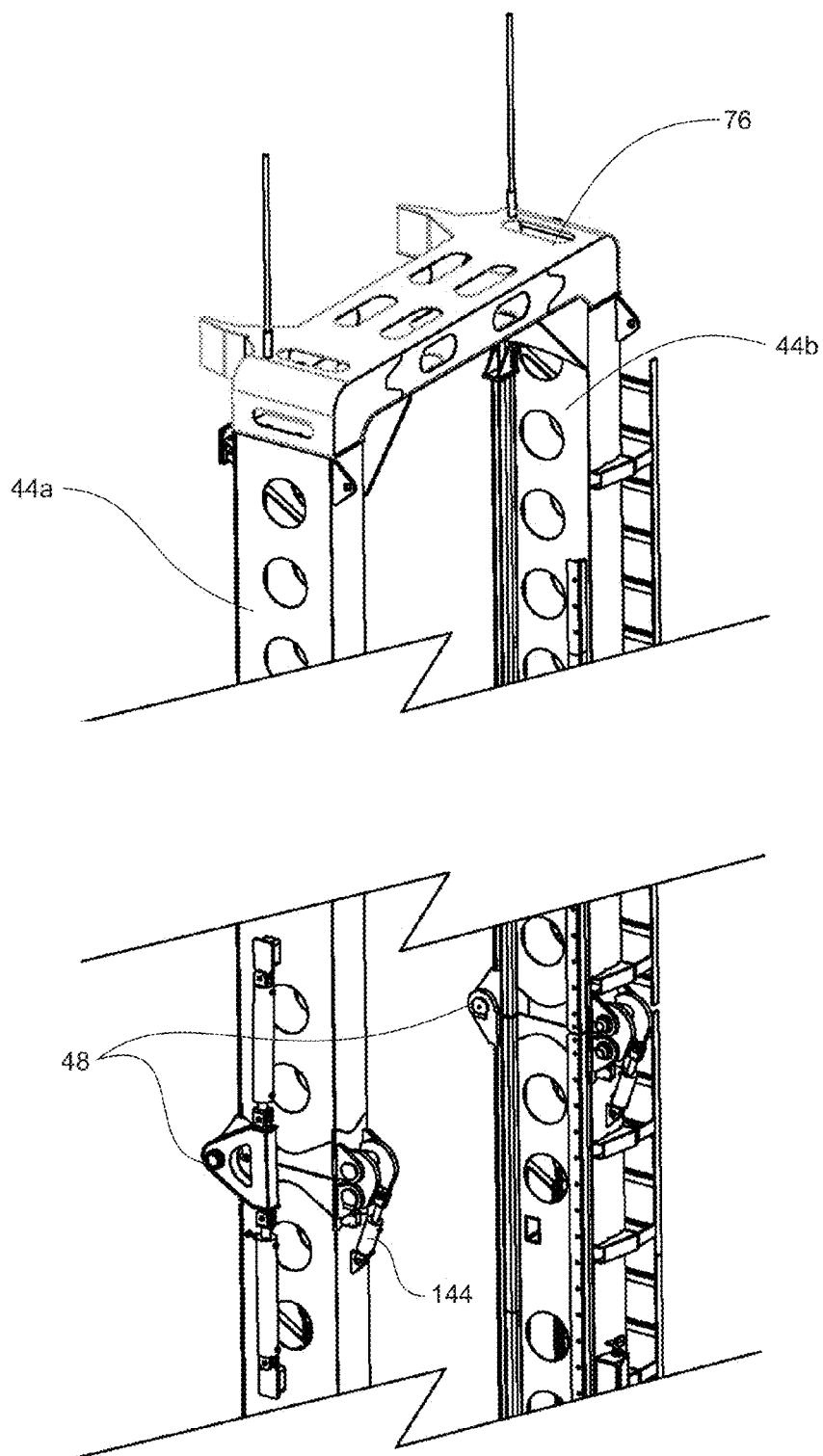
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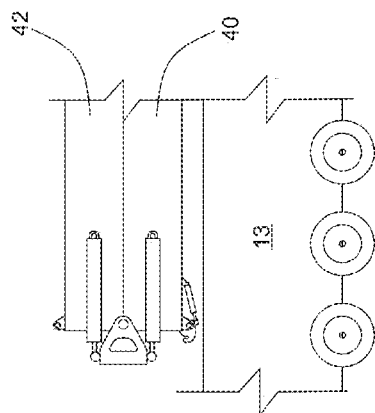
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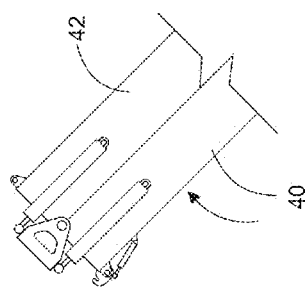
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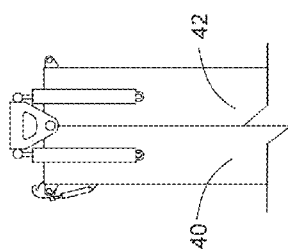
**Fig. 6**



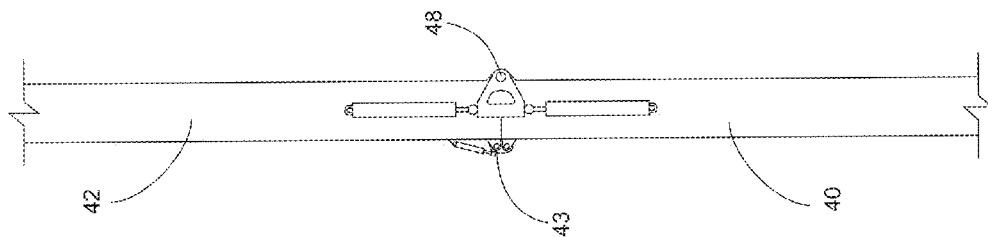
**Fig. 7A**



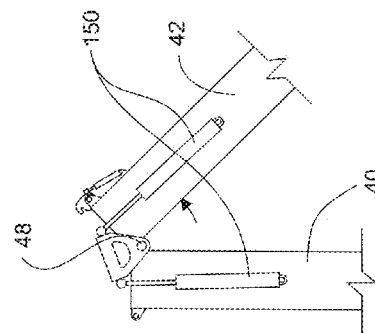
**Fig. 7B**



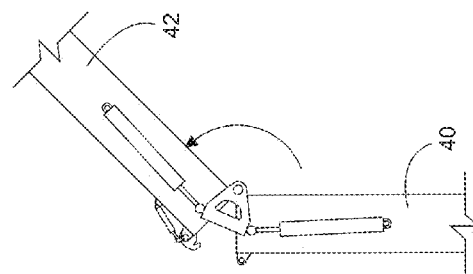
**Fig. 7C**



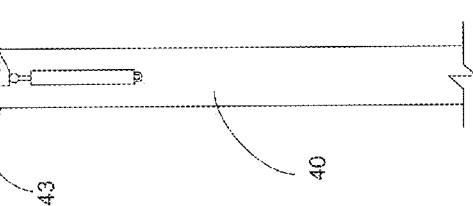
**Fig. 7D**



**Fig. 7E**



**Fig. 7F**



**Fig. 7G**

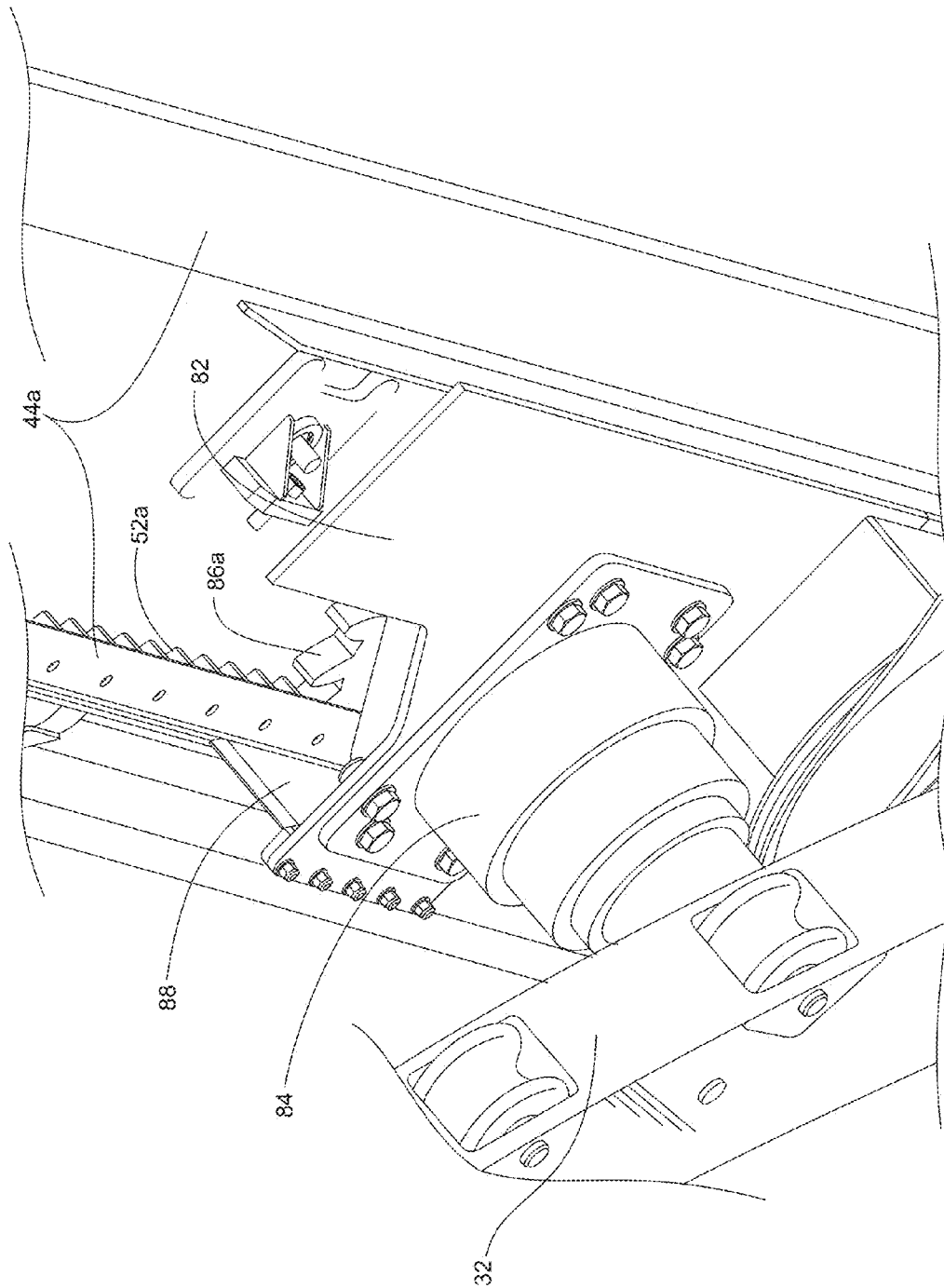


Fig. 8

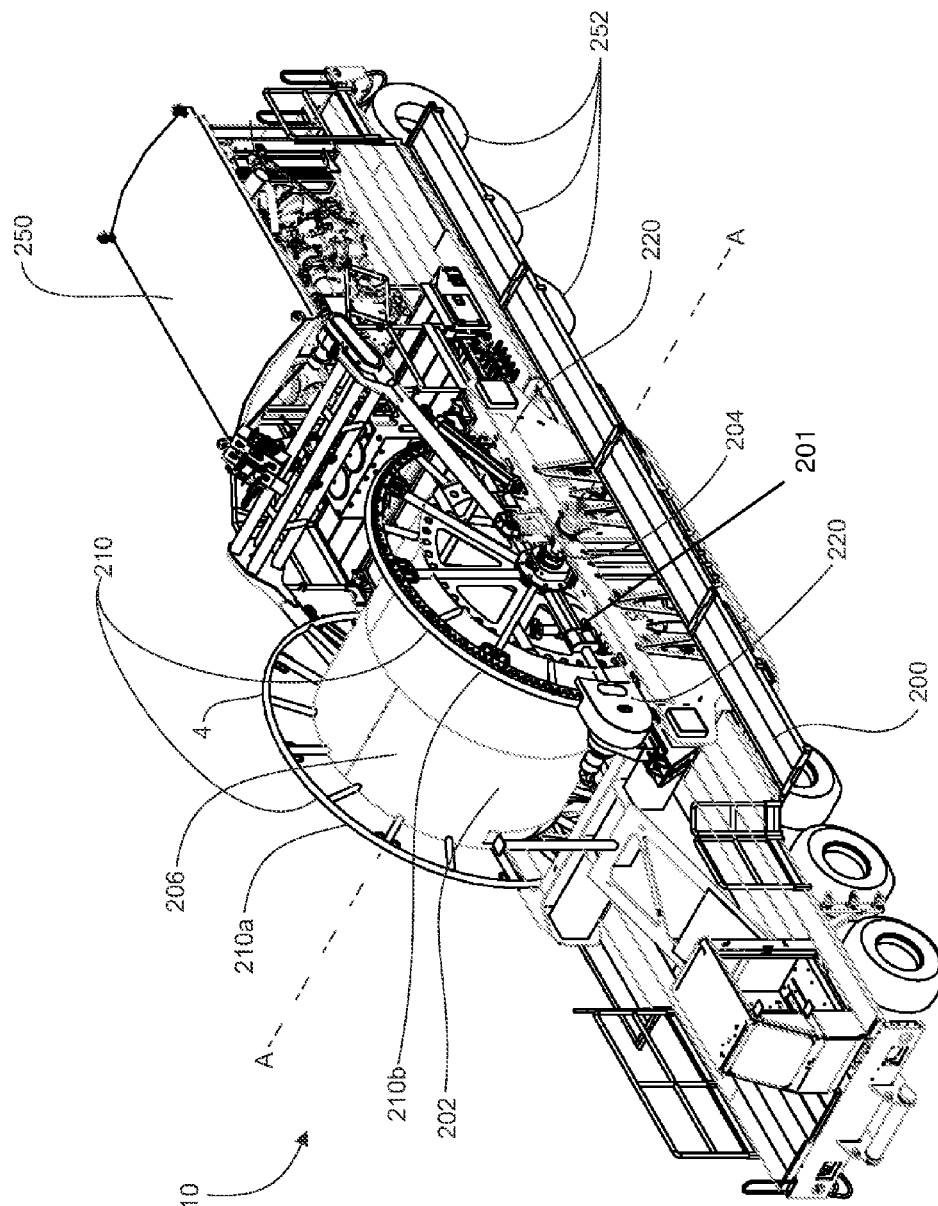
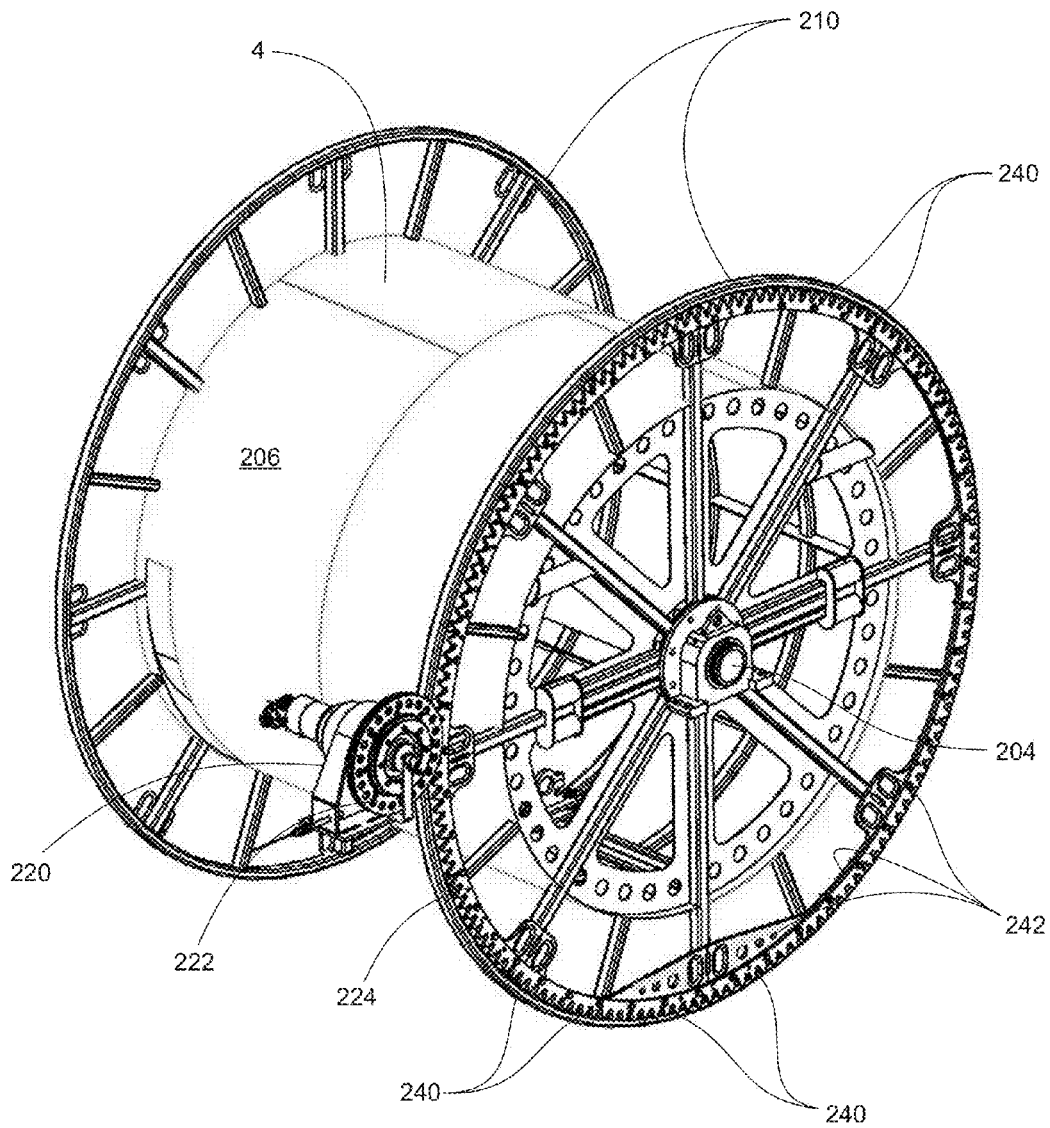


Fig. 9





**Fig. 10**

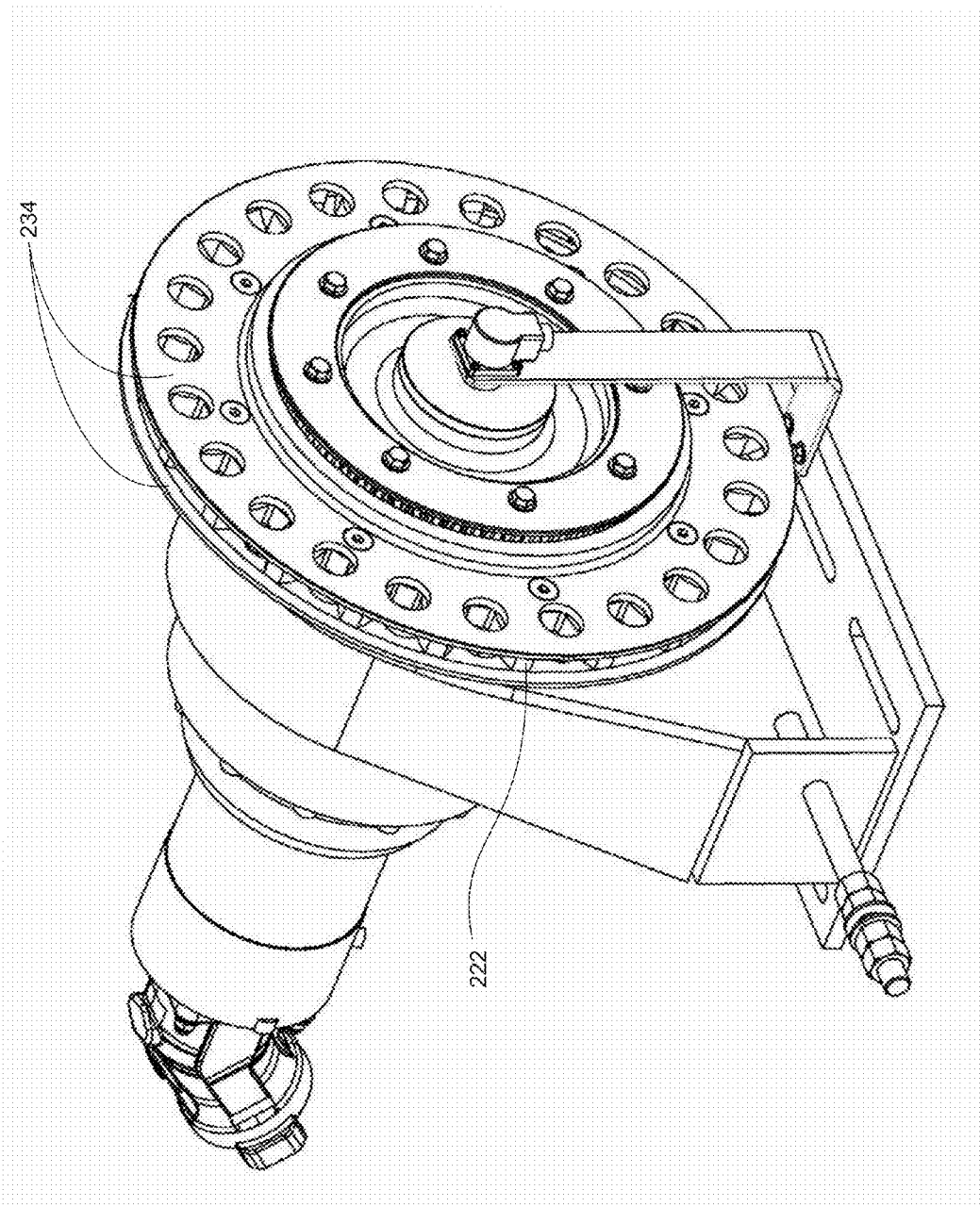


Fig. 11A

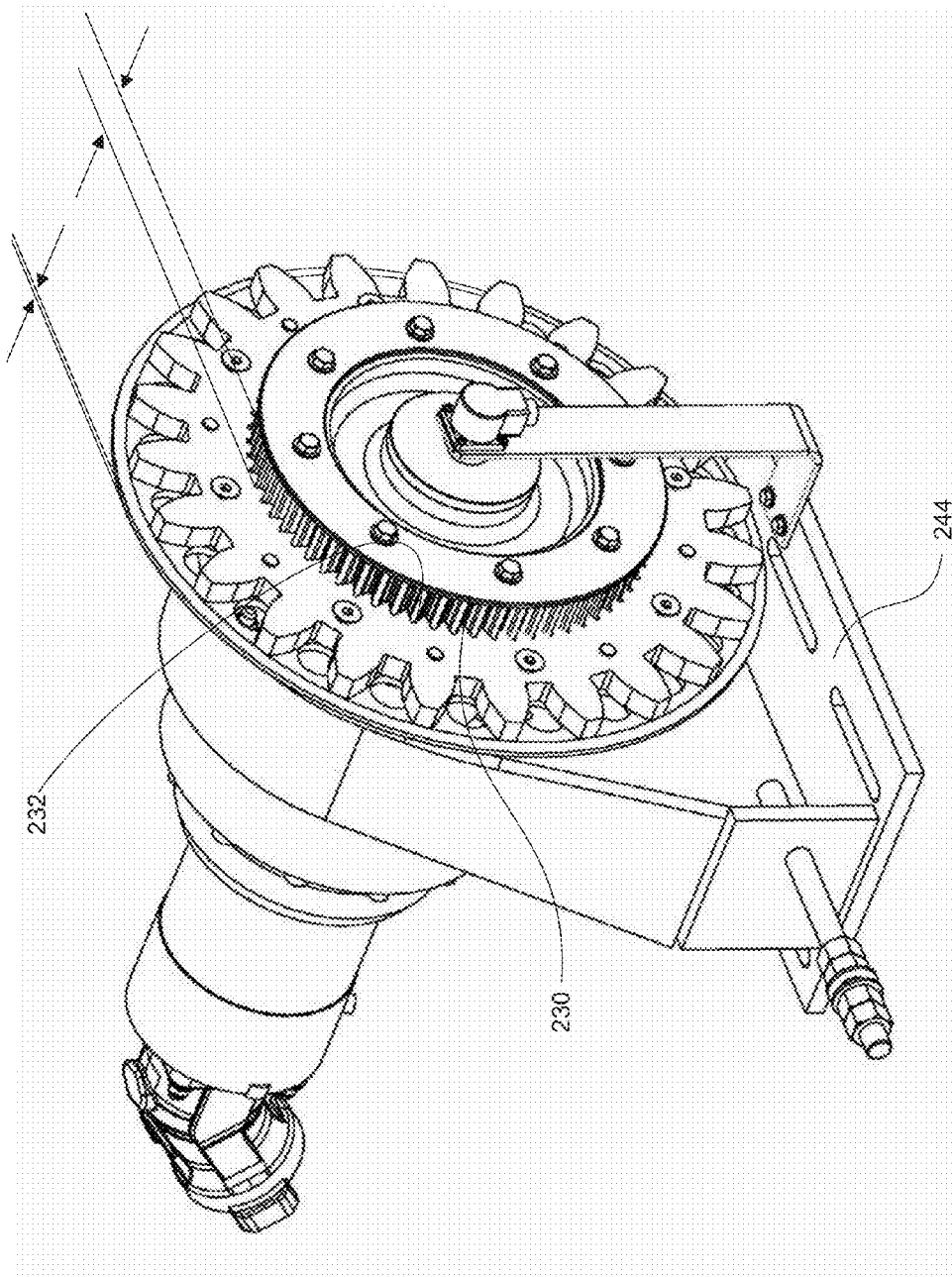


Fig. 11B

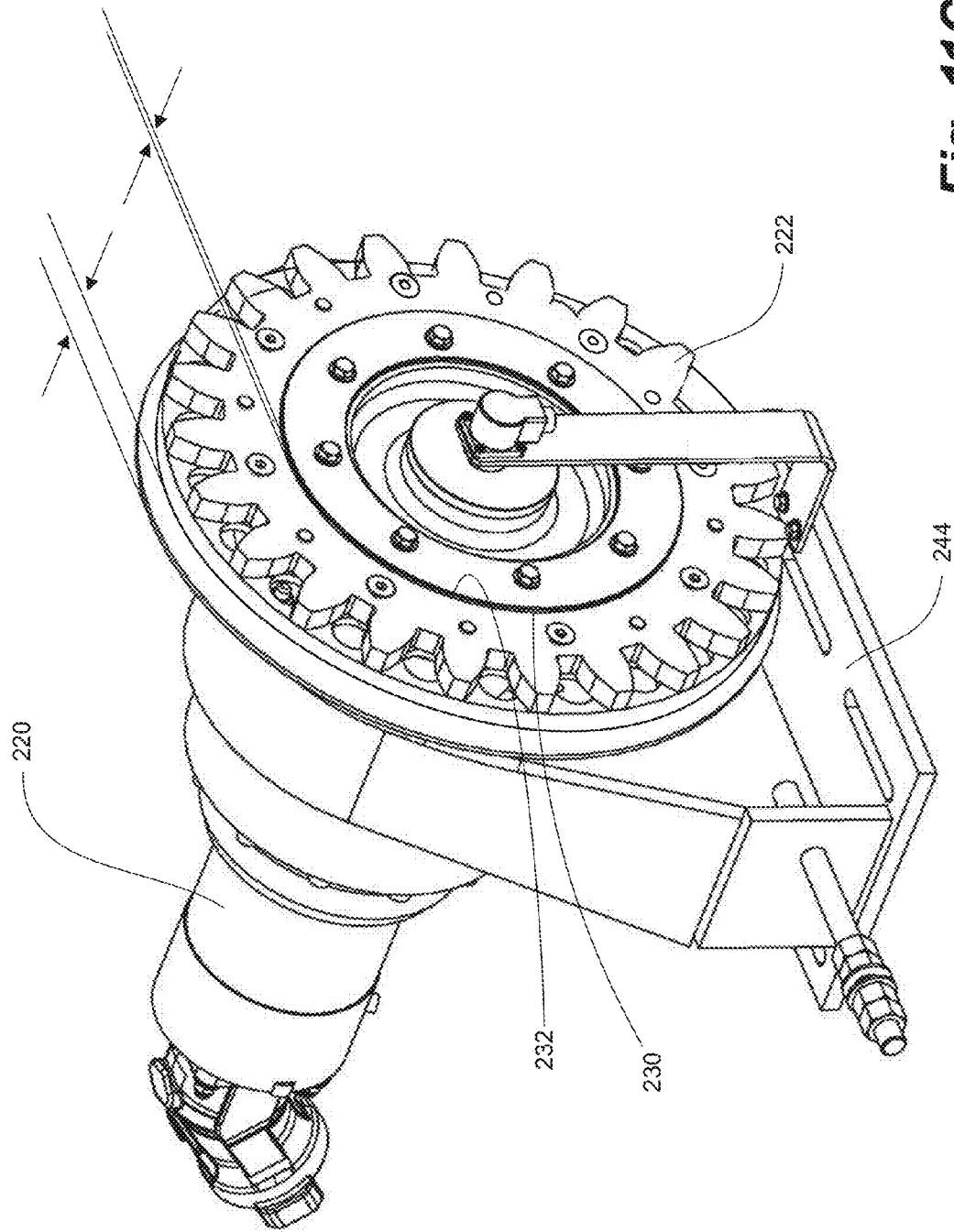
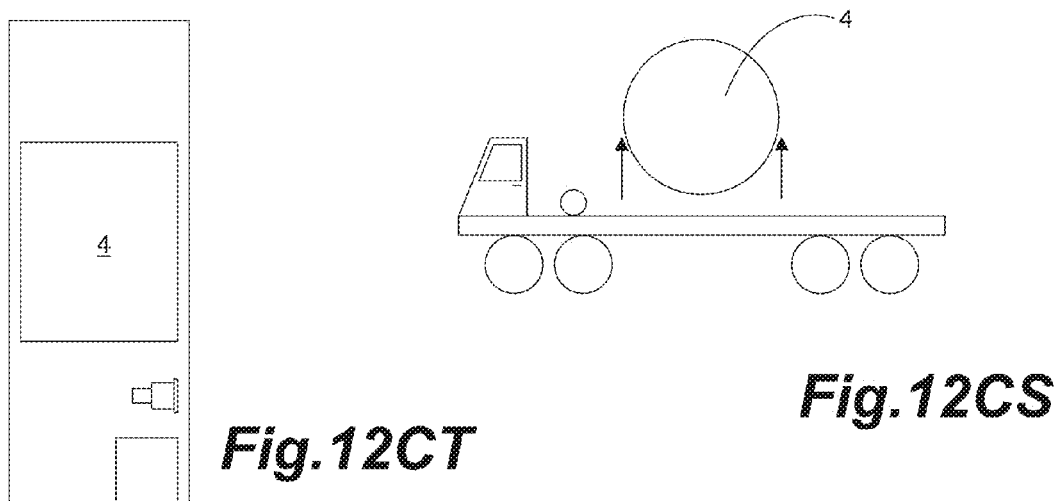
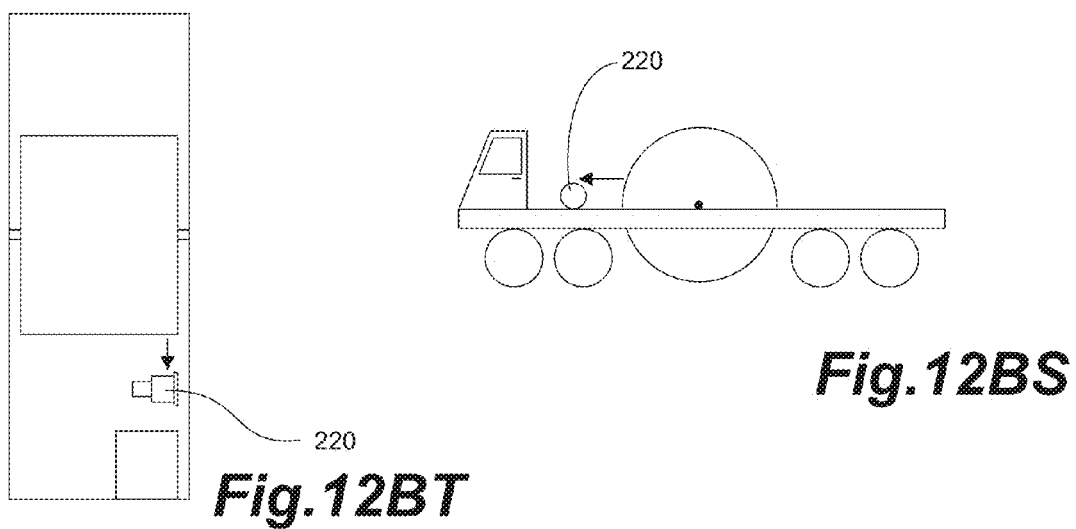
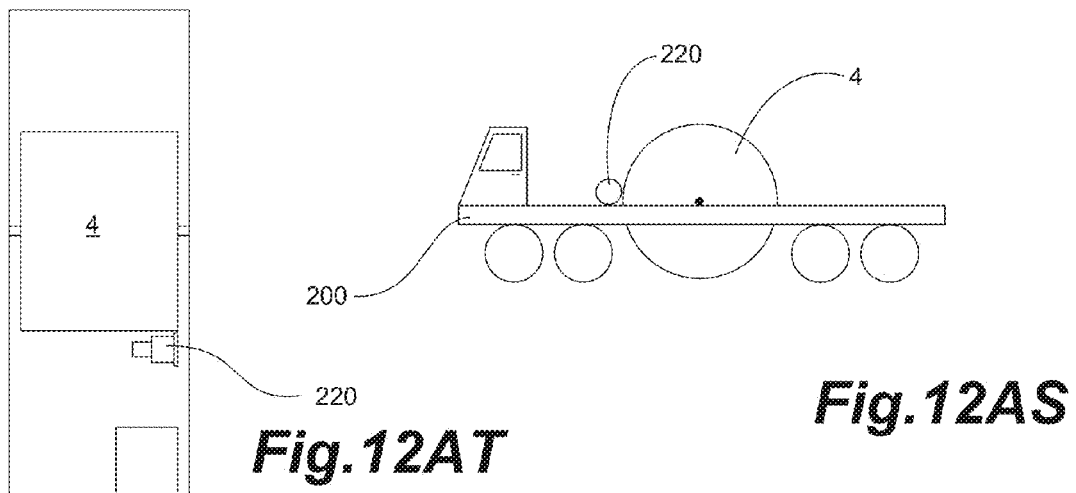
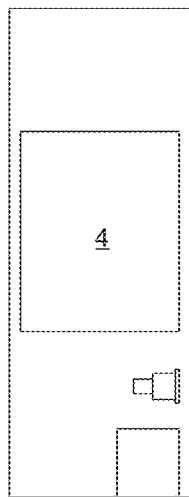
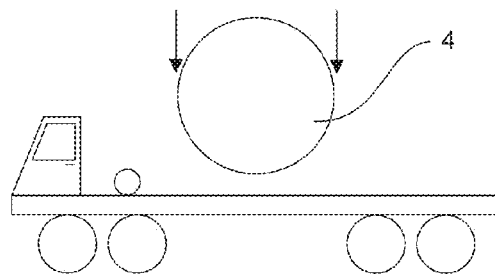


Fig. 11C

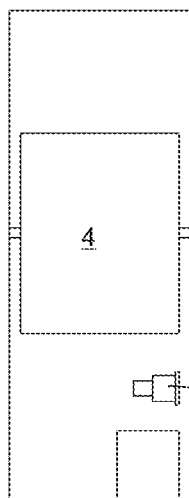




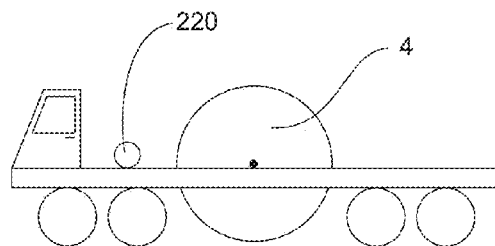
**Fig. 12DT**



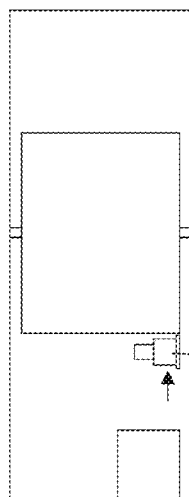
**Fig. 12DS**



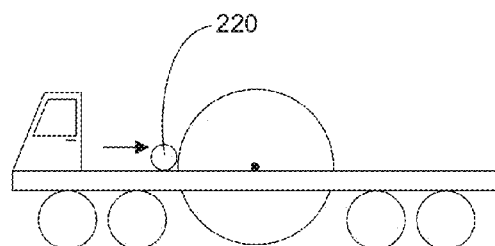
**Fig. 12ET**



**Fig. 12ES**



**Fig. 12FT**



**Fig. 12FS**

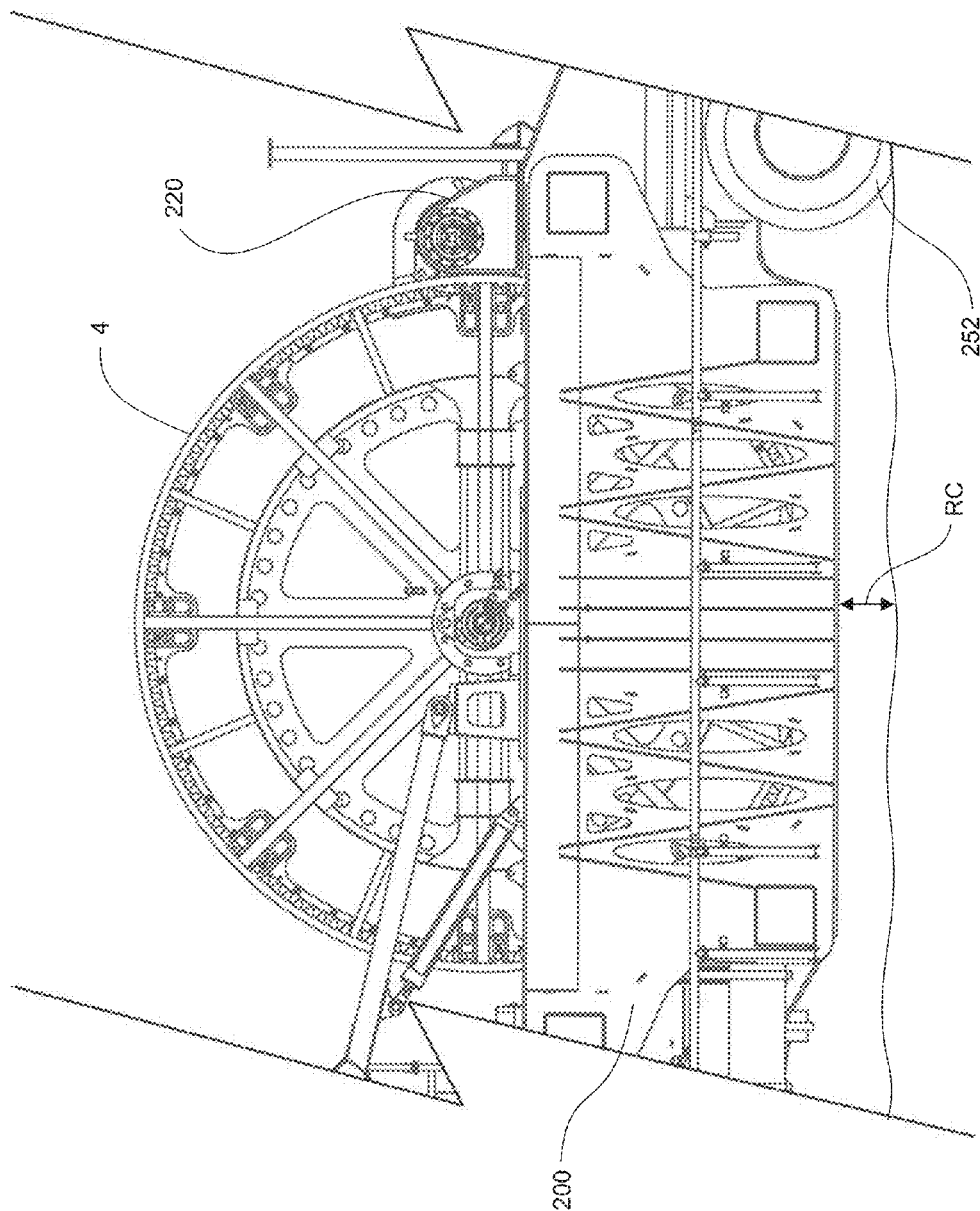


Fig. 13

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## MOBILE COILED TUBING REEL UNIT, RIG AND ARRANGEMENTS THEREOF

### CROSS-RELATED APPLICATIONS

This application claims the benefits under 35 U.S.C. 119(e) of the U.S. Provisional Application Ser. No. 61/666, 297, filed Jun. 29, 2012, which is incorporated fully herein by reference.

### FIELD

Embodiments described herein relate to a system for injecting coiled tubing into and out of a wellbore and supplying coiled tubing thereto. More particularly the system relates to versatile arrangements of a mobile injector unit having a reorientable gooseneck and separate mobile reel unit.

### BACKGROUND

Systems for injecting coiled tubing (CT) into and out of a well bore are well known, typically used for hydraulic fracturing operations. The majority of the known systems comprise an all-in-one trailer for supporting and positioning a coiled tubing injector supported in a mast, a coiled tubing reel and a control cab. The mast is erectable at a back end of the trailer over a wellhead, the reel being centrally located and the control cab located over the pin end of the trailer. The injector includes a gooseneck for guiding the coiled tubing into the injector from the reel. Drawworks, crown sheaves and cables position the injector and gooseneck in the mast at injection elevation. During running in and tripping out, CT is spooled on and off of the reel under control of an operator in the control cab. The CT can remain stabbed into the injector even during shipping.

Downhole operations demand longer and longer bottom hole assemblies (BHA's) which require longer/taller lubricators and require positioning of the injectors at a greater overall height or elevation above the wellhead. Further, as wellbores become longer and longer for maximizing access to deeper hydrocarbon payzones, the longer lengths of CT require larger reels, resulting in combined reel and trailer weights being greater than weight allowances and negatively affect dimensions of CT permitted for conventional transport.

More frequently, current systems are limited in regards to maximum injector elevation due to constraints upon limitations on the transportable length of the mast and the weight of the rig. Thus, a length of CT that can be carried with the rig is limited to accommodate transport or road allowances.

When masts are fit with deployable extensions, operations or length are compromised due to the difficulty in creating a continuous track through the extension, upon which the injector is to be raised and lowered.

Thus, there is interest in apparatus and methods for increased mast height for handling longer BHA's and for maximizing reel capacity while retaining the ability for meeting conventional road allowance requirements.

### SUMMARY

Embodiments described herein relate to a system for injecting coiled tubing into and out of a wellbore. Generally, a system and particular arrangements of apparatus are provided for injecting coiled tubing (CT) into and out of a wellbore to overcome limitations found in prior art systems.

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Embodiments of a mobile injector unit are fit with a mast configuration that enables higher elevations and therefore can accommodate taller lubricators. Further, the injector unit is freed of the reel and associated weight. Instead, in 5 embodiments a separate reel unit is provided, dedicated to reel transport for maximal reel capacity. In embodiments, a reel drive is provided for managing larger than conventional reel movement and facilitating spent reel removal and replacement reel installation.

Further, embodiments of the mobile injector unit and mobile reel unit enable flexibility of the layout on site, either guiding CT over the injector unit in a drive end orientation somewhat reminiscent to prior art all-in-one units, or alternatively in a back end orientation, with the CT being guided 10 from the wellhead side of the injector.

According to one broad aspect, a system is provided for conveying coiled tubing (CT) into and out of a wellbore comprising a first mobile unit having a first mobile frame having drive end, a back end and a mast supported on the back end adjacent the wellbore, the mast pivotable between a transport position and an erect position; a CT injector 15 moveable along the mast; a gooseneck; and a rotatable support between the gooseneck and the injector. A second mobile unit is also provided having a second mobile frame having a CT reel and a reel drive. Accordingly, when the second mobile unit is located at the drive end of the first mobile unit, the gooseneck is rotatable on the rotating support to the drive end to receive CT therefrom. Further, when the second mobile unit is located at the back end of the first mobile unit, the gooseneck is rotatable on the rotating support to the back end to receive CT therefrom.

The above system can be used in a method for injecting coiled tubing (CT) in and out of a wellbore, comprising positioning a CT injector unit with a back end adjacent a wellbore, an opposing drive end and a longitudinal axis, the CT injector unit having a mast supporting at least a CT injector and a gooseneck; positioning a CT reel unit generally in line with the longitudinal axis of the CT injector unit; rotating the gooseneck to receive CT from the CT reel unit; 20 supplying CT from the CT reel unit to the CT injector unit; and resisting loading applied to the mast.

In another aspect, a folding mast for a coiled tubing (CT) injector is provided. The folding mast is supported from a frame and comprises a pair of parallel mast posts. A carriage is supported between the mast posts and adapted for moving the CT injector along the mast, each mast post further comprising: a first mast section for support from the frame, a second mast section, and an extension pivot, pivotally connecting the second mast section to the first mast section. 25 A crown connects the second mast sections of each mast post.

Further, in another aspect, A rotating gooseneck can be provided comprising a rotatable support between the gooseneck and the CT injector. The gooseneck is foldable having a proximal segment of the gooseneck connected to the rotatable support, and a distal segment connected to the proximal segment and pivotable between an extended position for forming an arcuate CT guide, and a folded position. When the gooseneck is in the folded position, the folded gooseneck has effective turning radius that enables rotation clear of the mast.

In another aspect, a mobile unit for transporting a reel of coil tubing (CT) can be provided comprising a mobile frame having front and rear wheels and a transport envelope 30 having a height and width substantially that of road transport allowances. A CT reel is fit intermediate the longitudinal extent of the frame between the front and rear wheels and



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comprising a spool having an axle on a reel axis and bounding flanges, the width between the bounding flange being substantially that of the mobile frame, and the diametral extent being substantially that of the height of the transport envelope; and a drive is provided offset radially from the reel axis and engaging at least one of the bounding flange for rotation thereof.

A drive system for a mobile reel unit can further comprise a CT reel comprising a spool having an axle on a reel axis and bounding flanges; and a drive offset radially from the reel axis and engaging at least one of the bounding flange for rotation thereof.

#### BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1A is a schematic of an embodiment of the system for injecting coiled tubing into and out of a wellbore where a coiled tubing reel unit is aligned of the drive end of a coiled tubing injector unit on the same side of a well;

FIG. 1B is a schematic of an embodiment of the system for injecting coiled tubing into and out of a wellbore where a coiled tubing reel unit is spaced on a back end of the coiled tubing injector unit on opposing sides of a well;

FIG. 2A is a perspective view of a drive end view of an erect mast;

FIG. 2B is a perspective view of a back end view of the mast of FIG. 2A;

FIG. 2C is a partial perspective view of the locking clamp for the mast extension;

FIG. 3A is a perspective view of an embodiment of the coiled tubing injector unit while in a non operating configuration;

FIG. 3B is a perspective view of an embodiment of the coiled tubing injector unit while the mast is erected in an operating configuration;

FIG. 4 is a perspective view of an embodiment of an injector, injector carriage and pinion drive, and a gooseneck having the arcuate CT guide section in an extended position;

FIGS. 5AS through 5HT are pairs of simplified side (S) and top (T) views of a gooseneck and CT injector in a mast, the views illustrating in sequence how the gooseneck is reoriented from a drive side to a back end orientation, more particularly:

FIGS. 5AS and 5AT illustrate the gooseneck having the arcuate guide section extended in a drive end orientation;

FIGS. 5BS and 5BT illustrate the gooseneck in a folded position in preparation for reorienting from the drive end towards the back end orientation;

FIGS. 5CS and 5CT illustrate the gooseneck tilted approximately 60 degrees to the drive side from the injector;

FIGS. 5DS and 5DT illustrate the injector and gooseneck translated away from the mast to at least partially clear the mast;

FIGS. 5ES and 5ET illustrate the gooseneck partially rotated until interference with the mast;

FIGS. 5FS and 5FT illustrate the gooseneck tilted back towards the injector to clear the mast and complete the rotation to the back end;

FIGS. 5GS and 5GT illustrate the gooseneck tilted for securing to the injector and the injector translated back towards the mast;

FIGS. 5HS and 5HT illustrate the gooseneck arcuate guide section extended to the back end for operations;

FIG. 6 is a partial and perspective view of an embodiment of the parallel mast posts having the pivot, folding and a form of claw latch locking mechanisms of a folding mast according to one embodiment;

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FIGS. 7A through 7G are a series of partial side views illustrating the pivot or hinged portion of the folding mast according to FIG. 6, the base and extension portions of the mast shown in a sequence from transport to an erected position, more particularly:

FIG. 7A shows the mast folded and in the transport position on the rig;

FIG. 7B shows the base portion of the mast being raised;

FIG. 7C shows the base portion of the mast in the erect and folded position;

FIGS. 7D, 7E and 7F are three stages of the rotation of the distal extension end of the folding mast being raised to the extended and erected position; and

FIG. 7G shows the mast fully extended the lock claw of one portion engaging the lock pin of the other portion;

FIG. 8 is a perspective view of the rack and pinion system connecting the injector frame to the folding mast;

FIG. 9 is a perspective view of the mobile coiled tubing reel unit;

FIG. 10 is an isolated perspective view of an embodiment of the reel drive system, limited to the reel, bull gear and drive;

FIG. 11A is a perspective view of an embodiment of the drive and drive gear according to FIG. 10;

FIG. 11B is a perspective view of the drive gear of FIG. 11A, a side rail shown removed for viewing the gear shifted axially on a splined driveshaft towards the drive itself;

FIG. 11C is a perspective view of the drive gear of FIG. 11B, the gear shifted axially on a splined driveshaft away from the drive;

FIGS. 12AT through 12FS are pairs of schematics illustrating a top (T) view and a corresponding side (S) of steps taken to replace a reel on the coiled tubing reel unit of FIG. 9, more particularly:

FIGS. 12AT and 12AS are top and side views respectively of a CT reel ready for replacement;

FIGS. 12BT and 12BS are top and side views respectively of the drive and drive gear displaced longitudinally, and radially away from the reel' bull gear;

FIGS. 12CT and 12CS are top and side views respectively of reel being removed from the coiled tubing reel unit;

FIGS. 12DT and 12DS are top and side views respectively of a new reel being installed into the coiled tubing reel unit;

FIGS. 12ET and 12ES are top and side views respectively of the new reel in place in the coiled tubing reel unit;

FIGS. 12FT and 12FS are top and side views respectively of the drive and drive gear being returned longitudinally and radially into engagement with the bull gear; and

FIG. 13 is a side view of the support structure about the reel in the mobile frame for achieving maximal reel diameter.

#### DESCRIPTION

A system is disclosed for injecting coiled tubing (CT) into and out of a wellbore.

In FIGS. 1A and 1B, embodiments of the system comprise two separate mobile units used for injecting coiled tubing 2 (CT) into and out of a wellbore (wellbore not shown). A first coiled tubing injector unit 12 is provided on a first mobile frame 13, absent a CT reel, in favour of a second mobile CT reel unit (CTRU) 10, on a second mobile frame 200, having a reel 4. In embodiments described herein, the CT reel unit 10 can accommodate a large CT reel 4, permitting larger and longer CT for use in extended length downhole operations.

Accordingly, embodiments of the invention are adaptable for deploying a greater variety of CT having various diameters, lengths and weights.

Further, and as illustrated by the opposing arrangements of the units 12, 10 of FIGS. 1A and 1B, as a result of various physical space constraints that may be present at various well sites, embodiments are adaptable to permit the CT 2 to be injected from either a front end or drive end 33 or a back end 19 of the CT injector unit 12.

Referring to FIG. 1A, in an embodiment, the CT injector unit 12 comprises a mast 16, pivotably supported at a mast pivot 18 at a wellhead or back end 19 of the unit 12. An injector 22, having a gooseneck 26, is supported on the mast 16 and is moveable therealong for injecting CT 2 into a wellbore. The injector 22 overhangs the back end 19 and, in part, counteracts the loading of the CT 2 being feed thereto. As disclosed in greater detail below, a mast support 30, such as a tensile load-resisting member, connecting the mast 16 to the injector unit 12, resists or counteracts load from any overturning moments imposed by the delivery of CT 2 to the injector 22. Further, an optional tensile member, such as a guy wire 31, connects a top end 32 of the mast 16 with a front or drive end 33 of the CT injector unit 12 for providing additional stability to the mast 16 when erect. As shown, the CTRU 10 comprises the CT reel 4 having CT 2 wound thereabout for supplying CT 2 for injecting into the wellbore. As shown, the CT 2 is guided into the injector 22 by the gooseneck 26 supported on the injector 22.

More specifically, as shown in FIG. 1A, in one embodiment, the CTRU 10 is positioned at the back end 33 of the CT injector unit 12. The gooseneck 26 is oriented to face the CTRU 10 in a first, drive end orientation.

In an alternate embodiment, and as shown in FIG. 1B, the CTRU 10 is positioned in a back end orientation at the back end 19 of the CT injector unit 12, supplying CT from the injector side of the mast 16. In this orientation, the injector unit 12 and reel unit 10 are on opposing sides of the wellhead. In this embodiment the gooseneck 26 is pivoted to face away from CT injector unit 12. The weight of the injector 22 compounds the loading of the supplied CT 2. The guy wire 31 resists or counteracts the overturning load on the mast 16.

A person of ordinary skill in the art would understand that, unless otherwise detailed, both the CTRU 10 and the CT injector unit 12 would comprise various support equipment typically found on conventional apparatus.

With reference to FIGS. 2A and 2B, the mast 16 is mounted for pivotal movement on the back end 19 of the CT injector unit 12. The mast 16 comprises a pair of spaced, longitudinally extending and parallel mast posts 44a, 44b.

Each post 44a, 44b has a base or first mast section 40 and an extension or second mast section 42. A first or proximal end of the first mast section 40 is pivotally mounted at mast pivot 18 to the CT injector unit 12 while an opposing second or distal end is pivotally connected at the extension pivot 48 to the second mast section 42. The mast posts 44a, 44b are connected at crown 76. The base and extension portions 40, 42 are secured in the extended position using a mast lock 46.

As shown in more detail in FIG. 2C, and illustrated in the latched or locked position, the mast lock comprises a releasable clamp 43 used for securing the first and second mast sections 40, 42 together to ensure the folding mast 16 sections become, and temporarily remain, unitary during operation. In one embodiment, each releasable clamp 43, opposing each extension pivot 48, comprises a fold lock claw 140, a latch pin 142, and a claw actuator 144. The latch pin 142 may be connected to either the first or second mast section

40, 42, while the fold lock claw 140 is pivotally connected to either the opposing second or first mast section 42, 40, opposite the pin 142. Each claw 140 is pivotally connected to its respective mast section 40, 42 at a claw pivot 146 and actuator 144, such as a hydraulic ram, rotates the claw 120 about the claw pivot 146 between two positions, firstly to lock the mast extension, by engaging a claw hook 148 with the latch pin 142, and secondly to disengage the hook 148 from the latch pin 142 to permit folding of the mast 16.

A pair of hydraulic rams 50, 50 act to raise the base or first mast section 40 into an erect, operating configuration. The extension or second mast section 42 typically remains folded onto the first section 40 in a non-operating position. Each mast post 44a, 44b is fit with facing toothed racks 52a, 52b for incorporating a rack and pinion injector positioning system for selectively elevating the injector 22 along the length of the mast 16. As discussed for the configuration of FIG. 1A, loading applied to the mast 16 by the drive end CT supply imparts an over-turning load on the mast 16. Tensile releasable struts 60, 60 act to resist the over-turning load (one strut 60 per mast post 44a, 44b). Mast over-turning loads are transferred through the struts 60, 60 into the structure of the mobile injector unit 12.

Having reference to FIG. 3A, the injector unit 12 is shown configured in a non-operating configuration, with the mast 16 in a stowed position, the posts 44a, 44b substantially parallel to a mobile frame 13 of the injector unit 12 for transport. The gooseneck 26 and injector 22 are moved low in the mast 16 for transport.

In FIG. 3B, the injector unit 12 is shown configured in an operating configuration, with the mast 16 raised into a substantially vertical or erect position for injecting CT 2 into and out of a wellbore.

Having reference to both FIGS. 3A and 3B, the injector 22 is supported on the wellbore side of the mast 16. The gooseneck 26, provided for guiding the CT 2 to and from the CTRU 10, is rotatably connected atop the injector 22 for reorienting between a drive end configuration, for accepting supplied CT 2 from the CTRU 10, or the back end configuration, for accepting supplied CT from the wellhead side. A driver's cab 70 and power plant 72 can be fit at the drive end 33. The frame has a longitudinal axis between the front and back ends 33, 19. The power plant 72 powers at least the self-propelled mobile frame. The driver's cab 70 and power plant 72 are lodged to advantage between the parallel mast posts 44a, 44b when the mast 16 is stowed for transport. Further, a control cab 74 is located intermediate the injector unit 12, or mid-unit, and is spaced from the power plant 72 to as to accommodate the crown 76 of the folded mast 16. During transport, the control cab 74 is straddled by the pair of spaced longitudinally extending parallel mast posts 44a, 44b. Accordingly, the control cab 74 is located intermediate the crown 76 and the back end 19 when the mast 16 is in the folded, transport position.

With reference to FIGS. 4 and 8 the injector 22 is mounted to a carriage 82 that is raised and lowered in the mast 16. The gooseneck 26 is rotatably connected to the injector 22 at a rotating support 80, such as a conventional plate, pin and pivot structure, not detailed herein. The rotational support 80 enables re-orienting of the gooseneck 26 so as to receive CT 2 from different directions. The gooseneck 26 has an effective turning radius which is quite large and would typically result in interference with the mast 16. The effective turning radius is manipulated by a combination of at least a folding of the gooseneck 26, translation of the gooseneck 26 away from the injector 22 and angular manipulation of the gooseneck 26 from the injector 22.

The carriage **82** supports the injector **22** and one or more drives **84** for opposing pinions **86a, 86b**. The pinions **86a, 86b** engage their respective racks **52a, 52b** along the mast posts **44a, 44b** for driving the carriage **82** up and down the mast **16**. The carriage **82** further comprises slides **88** which cooperate with the mast posts **44a, 44b** for stabilizing the carriage **82** relative to the mast **16** and aiding movement therealong.

The carriage **82** further incorporates an injector frame **90**, positioned between the carriage **82** and the injector **22**, and movable away from and towards the mast **16**. The injector frame **90** thus enables translation of the injector **22**. The injector frame **90** is actuated using a lateral actuator **92**, such as a hydraulic cylinder. The injector frame **90**, when moved away from the mast **16**, aids in shifting the effective turning radius of the folded gooseneck **26** so as to be clear of the mast posts **44a, 44b**.

The rotating support **80** further comprises a guide socket structure **94** supported thereon having a gooseneck pivot **96**, such as a pivot pin, pivotally coupling a proximal segment **32** of the gooseneck **26** to the rotating support **80**. The guide socket structure **94** further comprises a guide lock **98**, such as a locking pin, spaced from the gooseneck pivot **96** for securing the proximal segment **32** to the support **80** when it is desired to fix the gooseneck **26** to the injector **22**, and removeable when the gooseneck **26** is to be pivoted about pivot **96**. When locked, the guide lock **98** extends through both the guide socket structure **94** and the proximal segment **32**, preventing tilting of the proximal segment **32**. When the guide lock **98** is released, the proximal segment **32** is rotatable about guide pivot **96** to tilt the gooseneck **26**. The gooseneck pivot **96** aids in moving, adjusting or shifting the effective turning radius of the folded gooseneck clear of the mast posts **44a, 44b**.

With reference to FIGS. 5AS through 5HT the gooseneck **26** can be reoriented from the drive end orientation to the back end orientation. The gooseneck **26** is mounted at the rotating support **80** to the CT injector **22**. The gooseneck **26** normally extends between the pair of spaced and parallel mast posts **44a, 44b**. Therefore, without some accommodation, the gooseneck **26** would not readily rotate freely without risk of interference with the one or the other of the mast posts **44a, 44b**.

Accommodation is provided by a combination of at least a folding of the gooseneck **26** and rotation of the gooseneck **26** about the CT injector **22**. Accommodation can be further aided by a tilting of the gooseneck **26** and a translation of the gooseneck **26** away from the mast **16**.

Accordingly, for configuring the system between the drive end and a back end configuration, the gooseneck **26** can be manipulated for re-orienting above the CT injector **22**. Having reference again to FIG. 4, the gooseneck **26** comprises a base **100**, and an arcuate guide **102** comprising the proximal segment **32** adjacent the base **100** and a distal segment **34** extending away from the base **100** towards the CT reel **4**. The distal segment **34** is pivotally connected to the proximal segment **32** at an intermediate guide pivot **103** for folding the arcuate guide **102** upon itself.

The gooseneck base **100** is connected to a top of the CT injector **22** at the rotating support **80**. The distal and proximal segments **32, 34** of the arcuate guide **102** fold to minimize their storage volume for transport but also to minimize the effective turning diameter or turning radius when rotated.

The proximal segment **32** is pivotally attached at the guide socket structure **94** which is integrated into the base **100** for tilting of the gooseneck **26**. When secured, such as in use for injecting CT, the proximal segment **32** is bedded

into the guide socket structure **94** and the guide lock, such as a locking pin **98**, secures the proximal segment **32** to the base **100** to prevent rotation.

In this embodiment, the locking pin **98** extends through both the socket structure **94** and the base **100** of proximal segment **32**, preventing tilting. When the guide locking pin **98** is released, the proximal segment **32** is rotatable about gooseneck pivot **96**. Accordingly, when folded, the arcuate guide **102** can be tilted with respect to the injector **22** to manipulate the proximal or distal segments **32, 34** relative to the mast posts **44a, 44b**. When the effective turning radius of the folded arcuate guide **102** is not compact enough to clear the mast **16**, the gooseneck **26** can be tilted at the appropriate point of rotation.

As stated, the gooseneck **26** is re-positionable, by rotation, between the drive end and the back end configuration. The injector unit **12** and mast **16** are best able to resist CT loading substantially in line with the longitudinal axis of the injector unit **12**, either towards, or away from, the injector unit, as described below. One can determine a safe angular tolerance either side of the longitudinal axis.

Accordingly, herein, rotation of the gooseneck **26** is described in the context of rotation from the drive end orientation, in line with the injector unit **12**, to the back end orientation, in line with the injector unit **12**.

Having reference to FIGS. 5AS and 5AT, the gooseneck **26** is shown initially oriented in line with the injector unit **12**, mounted above the injector **22**. The gooseneck **26** extends generally between the longitudinally extending parallel mast posts **44a, 44b** and is oriented towards the injector unit **12**. When CT operations are to be conducted from the back end **19** of the injector unit **12**, the gooseneck **26** is rotated. Without accommodation, the gooseneck **26** cannot rotate out of the mast **16**. The mast **16** can be an encumbrance to manipulation of the ungainly gooseneck **26** and thus a system and method is provided for enabling conversion from drive end to back end operations. The proximal segment **32** is locked using locking pin **98** to prevent rotation about support **80**.

Having reference to FIGS. 5BS and 5BT, the gooseneck **26** is folded at the guide pivot **103** between proximal segment **32** and a distal segment **34**, reducing the gooseneck's effective turning radius. A gooseneck actuator **110**, such as a hydraulic ram, is provided for manipulating the distal segment **34** relative to the proximal segment **32**. One end of the actuator **110** is pivotally mounted to the rotating support **80** and extends along a chord for pivotal connection to the distal segment **34**. To fold the arcuate guide **102**, the actuator **110** is retracted, pivoting the distal segment **34** relative to the proximal segment **32** about the guide pivot **103**. When folded, a strut, shipping linkage or fold lock **112** is installed between the proximal segment **32** and the distal segment **34** of the gooseneck **26**, to retain the gooseneck **26** in the folded position during shipping and during further orientation maneuvers.

Turning to FIGS. 5CS and 5CT, when the effective turning radius of the folded gooseneck **26** is greater than the inside, side-to-side clearance between the sides of the parallel mast posts **44a, 44b**, the gooseneck **26** is tilted at the gooseneck pivot **96** at the rotating support **80**. To minimize a rotating radial sweep area or effective turning radius of the folded gooseneck **26**, the locking pin **98** is temporarily retracted or removed to permit the gooseneck **26** to be tilted partially out from between the sides of the mast **16**. The actuator **110** is used again, extending to rotate the folded gooseneck **26** about the gooseneck pivot **96**. The fold lock

112 maintains the gooseneck's folded position and thus, when the actuator 110 is extended, the folded gooseneck 26 is caused to tilt.

Thus, the actuator 110, in conjunction with the gooseneck pivot 96 and locking pin 98, first enables positioning of the gooseneck 26 between the extended position (FIG. 5AS) and the folded position (FIG. 5BS). The extended position permits operations for guiding CT 2. The folded position is used for shipping, transport and rotating. Secondly, the actuator 110 tilts the folded gooseneck 26 about the gooseneck pivot 96 to provide additional clearance between the distal segment 34 of the gooseneck 26 and the mast posts 44a, 44b permitting rotation of the gooseneck 26.

As shown in FIGS. 5DS and 5DT, for additional clearance, the injector 22 is then displaced laterally away from the parallel mast posts 44a, 44b. The CT injector 22 is displaced or translated away from, and towards, the mast 16 by displacing the injector frame 90 using the lateral positioning member 92 such as a hydraulic cylinder. Thus, the distal segment 34 of the gooseneck 26 is displaced, as needed, from between the parallel mast posts 44a, 44b, and as a result, the distal segment 34 of the gooseneck 26 is free to rotate without interference by the mast 16.

With reference to FIGS. 5ES and 5ET, the gooseneck 26 is rotated using the rotating support 80 to re-orient the arcuate guide 102 to the back end orientation. As shown, as tilted, the proximal segment 32 of the gooseneck 26 when tilted can be rotated until it encounters interference by the mast 16, such as mast post 44a. As shown in FIG. 5ET, the gooseneck 26 is rotated about 90 to 120 degrees until the proximal segment 32 interferes with the mast post 44a.

During the rotation or when interference is detected, the actuator 110 is retracted to lessen the angle of tilt of the gooseneck 26 for spacing the proximal segment 32 further from the dual folding masts 44a, 44b, clearing the rotational path and enabling completion of rotation thereof.

As shown in FIGS. 5FS and 5FT, the gooseneck 26 is then rotated the balance of the rotation from the drive end orientation to the back end orientation, about 180 degrees in total. The locking pin 98 can be inserted before or after rotation.

At FIGS. 5GS and 5GT, the injector 22 is then laterally repositioned towards the mast 16.

Having reference to FIGS. 5HS and 5HT, once the injector 22 is retracted into the carriage 82 and oriented in the back end orientation for CT operations, the fold lock 112 is removed. The actuator 110 is used to extend the distal segment 34, to unfold and form the arcuate guide 102. The arcuate guide is then locked in the unfolded position for operations in the back end orientation.

In greater detail, and returning to FIGS. 2A, 2B, 3B, the folding mast 16 has an extension pivot point 48 intermediate its extended or erect length. The entirety of the mast, having significant height, fits on a single roadable, mobile platform or frame 13. The folding mast 16 is hydraulically lifted and support structure is provided to resist supplied CT loading without need for or overloading the hydraulic lifting mechanism. The mast 16 is folded and unfolded in two stages. Once fully unfolded to the extended position, the locking clamp 43 is engaged to ensure the folding mast becomes structurally unitary. As a result, the folding mast 16 has a useful injector-to-ground height in the order of about 50 feet, yet remains foldable for transport to less than about 40 feet in length.

The control cab 74 is positioned about mid-carrier, straddled by the mast 16 during transport.

The entirety of the mast 16 can be lifted from the non-operating configuration of FIG. 3A to the operating configuration of FIG. 3B using the pair of hydraulic rams 50, 50 connected between the first mobile frame 13 and the first mast section 40. In the operating configuration of FIG. 3B the first and second mast sections 40, 42 longitudinally align in a substantially vertical orientation, such as a slightly inclined position to align the injector 22 over a wellhead. In the non-operating configuration FIG. 3A the second mast section 52 folds onto first mast section 50, resting on and adjacent to the mobile frame 13 of the injector unit 12.

With reference to FIG. 2C, 6, and FIGS. 7A through 7G, each extension pivot 48 comprises a pair of opposing, two-stage, first and second actuators 150, 150, such as hydraulic rams. The pivot 48 further comprises a generally triangular fulcrum 152, having three apexes, a first apex pivotally attached co-axially to the extension pivot 48 and the actuators 150, 150 at the other two opposing apexes. The actuators 150, 150 extend between the fulcrum 152 and their respective mast sections, each actuator 150 to the fulcrum 152 at second and third opposing apexes, each apex being spaced away from the extension pivot 48 so to provide the necessary actuation leverage. When the mast 16 is the folded position, the actuators 150, 150 are extended. As the actuators 150, 150 are actuated to retract, the second mast section 42 is pivoted about 180 degrees about mast pivot 48 until in line with the first mast section 40. In an alternative embodiment, there may be only one two stage folding pivot 48 on the parallel mast posts 44a, 44b.

Once the mast 16 is completely unfolded to the operating configuration, the releasable clamp 43 secures the first and second mast sections 40, 42 together to ensure the folding mast sections become, and temporarily remain, unitary during operation. As discussed above, in one embodiment, the releasable clamp comprises the fold lock claw 140 and the latch pin 142 are fit to either one of the first or second mast sections 40, 42.

In operation, and having reference to FIG. 2A and FIGS. 7A-7C the coiled tubing injector unit 12 enters a well site with the mast 16 in the folded, non-operating position. The pair of actuators 50, 50 (FIG. 2A) raise the first mast section 40 into an operating configuration while the second mast section 42 remains in a folded non-operating position.

With reference to FIGS. 7D through 7G, the pair of pivot actuators 150, 150 are then actuated either sequentially (serial two-stage, actuator 150 then actuator 150) or in unison (parallel two-stage 150 and 150) for raising the second mast section 42 into an operating configuration. If actuated serially, the two-stage folding pivot 48 rotates the second mast section 42 approximately half way, being zero to 90 degrees, in the first stage, and the remainder of the way, being 90 to 180 degrees, in the second stage. The first and second mast sections 40, 42 are longitudinally aligned in a substantially vertical position once in the operating configuration. The fold lock claw 140 is then engaged using the actuator 144 for engaging the latch pin 142, locking together the first and second mast sections 40, 42. Prior to folding the mast 16 to the non-operating configuration, the claw 140 is actuated to disengage from the pin 142, and the second mast section 42 is able to pivot into a folded position.

In an alternative embodiment, the second mast section 42 may be raised to the operating position prior to the first mast section 40 being raised so that the mast 16 is fully extended yet lying substantially horizontal and parallel to the movable mobile frame 13 of the injector unit 12 before lifting. The

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first and second mast sections **40,42** may then be positioned while extended into a substantially vertical position using the hydraulic rams **50,50**.

Therefore the mast **16** having first and second foldable mast sections **40,42** is provided having a useful injector-to-ground height of approximately 50 feet, yet foldable for transport to less than 40 feet.

The control cab **77** is positioned mid-carrier, and straddled by the mast **16** during transport.

Having reference to FIGS. **2A**, **2B** and **8**, prior art drawworks cabling for injector manipulation is eliminated through introduction of a rack and pinion, CT injector positioning system for selectively moving the injector **22** up and down, and along, the length of the mast **16**. Herein, the cable-less rack and pinion positioning system works particularly well with the folding mast **16**, substantially seamlessly bridging the folding mast's **16** intermediate mast pivot **48**. Applicant's experience is that the prior art rack and pinion drives, used for conventional drilling rigs handling full string weights, were an uncomfortable compromise between low gearing to manage full string loads and higher gearing for faster tripping operations. For CT operations, using embodiments described herein, rack and pinion drive ratios can be optimized for positioning of the injector **22** and managing the dead loads of the injector **22** and surface coil weights. Running loads are supported by the injector **22**, to the lubricator, to the wellhead.

In one embodiment, the pair of toothed racks **52a,52b** are mounted to extend along the parallel facing mast posts **44a,44b** for each of the first and second mast sections **40,42**. Each of the racks **52a,52b** are provided in two sections, corresponding to the respective first and second mast sections **40,42**. When the mast **16** is in the non-operating configuration the two sections of each of the racks **52a,52b** are separated and discontinuous along the mast **16**. In an operating configuration, ends of the two sections of each of the racks abut to form a substantially continuous toothed rack **52a** and **52b**, bridging their respective mast pivots **48**.

A pair of drives **84,84**, one per rack **52a,52b**, are mounted to the injector carriage **82** for selectively moving the CT injector **22** along the mast **16**. The pair of pinions or pinion gears **86a,86b** on the carriage **82** are craven by the pair of drives **84** for engaging the toothed racks **52a,52b**.

Having reference to FIGS. **1A**, **2A** and **2B**, for CT operations from the drive end orientation, a first tensile member, such as a releasable strut **60** for each mast post **44a,44b**, is provided for transferring loads into the mobile frame **13** of the injector unit **12**. The mast **16** pivots at its base at the mast pivot **18** at the back end **19** of the injector unit **12**. CT operations from the drive end of the injector unit **12** impart lateral pulling loads on the mast **16** at about the gooseneck **26**, and directed towards the drive end of the injector unit **12**. This loading can be partially offset by the dead load of the injector **22** on the opposing, wellhead side of the mast **16**. The mast-lifting actuators **50** can be used to impart a resisting force on the first mast segment **40**, resulting in a large bending moment in the mast **16**, at an intermediate lifting point **152**. Thus, for operations, the tensile releasable strut **60** is positioned between the back of the erect mast **16**, being the tensile surface of the mast **16** as a beam in bending, to the back end **19** of the mobile frame **13** of the injector unit **12**.

Having reference to FIG. **1B**, when the gooseneck **26** is re-oriented for back end orientation, the aforementioned loading scenario is reversed, the tensile releasable struts **60,60** no longer being effective in compression. Hence, the mast **16** is further supported using second tensile members

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such as guy wires **31** extending from the mast **16** to a point intermediate towards the front **33** of the mobile injector unit **12**. In one embodiment, the guy wires **31** extend from a point adjacent the crown **76** of the mast **16** to a point adjacent the drive end **33** of the injector unit **12** for resisting CT forces and injector dead load transferred to the mast **16**.

In an alternative embodiment, the guy wires **110** can also extend from alternate positions along the length of the mast **16** such as from a position adjacent the injector **22**.

Referring again to FIG. **3A**, and in one embodiment, the CT injector unit **12** may be self-propelled and remains within road weight and height allowances. The power plant or engine **72** provides at least power to wheels **160** for propelling or driving the unit **12** from well site to well site. The driving cab **70** is provided at the drive end **33**. The engine **72** can be located between the driving cab **74** and the control cab **74**. The control cab **74** is located about the middle of the injector unit **12**. The mast **16**, when positioned in the non-operating transport configuration, straddles the control cab **74**. The stowed mast **16** sits sufficiently low on the mobile injector unit **12** to remain within the transport envelope including road height allowances.

Having reference to FIG. **9**, the separate CT reel unit **10** (CTRU) is provided comprising a mobile frame **200** for transporting and supporting the reel **4** of CT **2**, the frame **200** also having a transport envelope, the height and width of which being substantially that of specified transport or road allowances. The reel **4** is located intermediate the frame **200** and has a maximized diametral extent that is accommodated in a support frame portion **201** in the frame **200** located between the front and rear wheels. The reel **4** can be removable and is rotatably connected through the support frame portion **201**. The reel **4** extends substantially the width of the frame of the CTRU **10**. The reel **4** is rotatable about an axle **204** having axis A, for spooling CT **2** onto and off of the reel **4**. A drive system **202** rotates the reel **4** about the axis A. As the CTRU **10** has a separate mobile frame **200**, site positioning of CTRU **10** remains flexible.

Coupled with the above injector **22** and a rotatable gooseneck **26**, and with the gooseneck **26** positioned in the drive end orientation, the CTRU **10** is generally located at the drive end **33** of the injector unit **12** with the CT **2** extending over the injector unit **12** and into the arcuate guide **102** of gooseneck **26** (see FIG. **1A**). This orientation requires an increased amount of real estate on one side of the wellhead than that typically required for coiled tubing operations in the prior art. The site lease may not permit end-to-end positioning of the injector unit **12** and CTRU **10** on one side of the wellhead. Accordingly, the CTRU **10** can be located on the opposite side of the wellhead, opposing the injector unit **12** (see FIG. **1B**) and thus the gooseneck **26** would be repositioned to the back end orientation.

The CTRU **10**, being separate from the injector unit **12**, is optimized for maximizing CT length or weight. Prior art CT rigs are constrained as to the amount of CT they carry due to limitations on the size of the reel incorporated in a unitary platform which must also include a mast and injector. The size of prior art reels, particularly their width, are also constrained by the available space between the parallel mast posts to enable the mast to lay down for transport.

In contradistinction, embodiments provided herein have a removable reel **4**, or cartridge, carried by its own CTRU **10** and can now maximize the length of CT and maximize CT capacity, by utilizing virtually the entirety of the width of the CTRU **10**. Further, maximum diameter can be achieved, being substantially that of the road height allowance. As

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described below, reel drive and mobile platform improvements enable such increase in capability.

In operation, prior art chain drives to the shaft of a reel have conventionally been placed laterally adjacent to the reel, axially spaced on one side thereof, limiting the width of the reel that can be fit to the frame. In an embodiment disclosed herein, known chain drives have been removed and replaced with a drive system for operating the increased capacity reel 4 from the periphery of the reel as opposed to the side thereof.

Having reference to FIGS. 9 to 13 the reel 4 is a spool having the axle 204 and a tubing drum 206 that is bounded by at least one bounding flange 210, typically a pair of bounding flanges 210a and 210b, between which the CT 2 is wound. The CT reel 4 fits intermediate the longitudinal extent of the frame between the front and rear wheels. The drive system 202 comprises a drive 220, such as a planetary drive, that drives the reel 4 about a periphery of at least one driven bounding flange 210. While a chain drive about the flange 210 would assist with maximizing reel width, further advantage is obtained by eliminating chains altogether.

With reference to FIG. 10, the drive 220 is radially offset from the reel axis A. The drive gear 222 drives a sprocket or bull gear 224 fit about flange 210. The drive 220 is supported upon the mobile frame 200 for driveably engaging the drive gear 222 with the bull gear 224. Therefore, need for a conventional, axially spaced chain drive and impact on width is eliminated. As the drive gear 222 is parallel and radially offset from the reel 4, spaced longitudinally along the CTRU 10 as opposed to spaced axially along the reel axis, the reel 4 can extend substantially the width of the frame 200, maximizing the reel capacity. Further, use of a drive and bull gear 222,224, eliminates chain breakage and associated risk to operators.

The mobile frame 200, such as that of FIG. 9, has an inherent flexibility, albeit minimal in the context of serving as transport apparatus, but which introduces challenges to maintaining engagement of drive gear 222 and bull gear 224. Engagement issues can include manufacturing tolerances and alignment, alignment including angular variations in the parallel offset of the drive gear 222 and bull gear 224.

In one aspect, as shown in FIGS. 11A, 11B and 11C, the drive gear 222 is fit with means for tracking the bull gear 224 or otherwise maintaining continuity of the drive system 202. As shown in FIG. 11A, the drive gear 222 is fit with axially spaced, radially extending side rails 234, 234, straddling the drive gear and hence straddling the bull gear 224 for tracking relative side-to-side movement therebetween, the side rails 234,234 maintaining engagement of the drive gear 222 and bull gear 224, despite flexing of the frame 200 of the CTRU 10. In one embodiment the drive 220 has a splined driveshaft 230. The drive gear 222 is fit with a splined bore 232 (FIG. 11B). The splined bore 232 of gear 222 is axially movable on the splined driveshaft 230. Thus, generally axial relative movement between the drive gear 222 and bull gear 224 are accommodated. Typically, side-to-side movement of the bull gear 224 engages the drive gear's side rails 234 and urges the drive gear 222 to move or shift correspondingly.

Having reference to FIG. 11B the interface of splined bore 232 and driveshaft 230 are illustrated, an outer side rail being omitted for illustrating the stroke of the splined movement. The gear 222 is shown shifted substantially completely towards the drive, or in this embodiment, inboard of the CTRU 10. As shown, the gear 222 can move outboard an amount approximately the same distances as that of the width of the gear 222 itself. With reference to FIG. 11C, when the side rail is present as in operation, the

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bull gear could have urged the gear 222 outboard to the extent of the splined portion of the driveshaft 230.

Referring to FIG. 10, and the reel 4 and bull gear 224 are manufactured with controlled tolerances to ensure proper engagement of the drive gear 222 and bull gear 224. The bull gear 224 can be manufactured in a plurality of gear sections 240,240 . . . and mounted to backing structure 242 arranged about the periphery of the reel 4. The arcuate sections 240 are each precisely machined and can be assembled, adjusted, and otherwise aligned to form a continuous bull gear on the backing structure 242. A precise gear can thus result on an otherwise less than precise foundation of the bounding flange 210. The reel 4 can be rotated on its axle 204 and any runout minimized through alignment of the sections 240, 240 . . . .

Further, the drive system 202 also accommodates removal of the reel 4 for replacement of spent reels or for maintenance.

Once the CT is spent or fatigued, the reel 4 of CT 2 can be replaced. To enable removal of the reel 4, such as by crane, the drive gear 222 and bull gear 224 need to be separated. Depending on the angle of the gear teeth, the drive 202 and drive gear 222 can be located low in the mobile frame 200, in about a lower quadrant of the reel's circumference, so that the gear teeth of the drive gear 222 and bull gear 224 separate cleanly upon an upward lifting of the reel 4 and axle 204 from the frame 200. The drive 220 and drive system 202 overall, could be difficult to maintain in this configuration. Alternatively, the drive 220 could be generally radially movable from an engaged position, to a disengaged position, releasing the drive from any locational constraints.

With reference to FIGS. 9, and 12A to 12F, the CTRU 10 is shown in various stages or steps for replacement of a reel 4. In FIGS. 12AT and 12AS the drive 220 and reel 4 are shown in an operational state with the drive gear 222 engaged with the bull gear 224. To enable removal, the drive gear 222 is shifted or displaced generally away from the reel 4. The drive 220 is mounted on a rail mount, slide mount or pivot for disengaging the drive gear 222 from the bull gear 224.

Herein, a form of slide mount 244 is provided for moving the drive generally radially between the engaged and disengaged positions. When the drive mount 244 is secure to the frame 200, the drive gear driveably engages the bull gear. When the drive mount 244 is released, the drive and drive gear are displaced sufficiently to release the reel for replacement. The extent to which the drive must be displaced depends upon the gear meshing and circumferential positioning of the drive about the driven bounding flange.

Accordingly, replacement of a reel 4 is as convenient as replacing a reel cartridge in a "plug-and-play" scenario.

As shown in FIGS. 12BT and 12BS, in one embodiment, the drive 220 is displaced generally radially away from the periphery of the reel 4, disengaging the drive gear 222 from the bull gear 224. Therefore, being free from the drive gear 222, and as shown in FIGS. 12CT and 12CS the reel 4 can be removed from the CTRU 10.

Note that the usual preparation for removal is performed including disconnection of fluid and electrical connections and release of the axle 204 from bearings associated therewith. Removal is improved over the prior art chain drives as chain separation and handling is no longer required.

As shown in FIGS. 12DT through 12ES, a replacement reel 4, such as that loaded with usable coiled tubing can then be installed on the CTRU 10.

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Finally, in FIGS. 12FT and 12FS, the drive 220 can then be displaced toward the reel 4 for engaging the drive gear 222 with the bull gear 224.

It is known to use a reel axis and axle as the drive connection of the CT reel. However, such use has limited the useful diameter of the reel's rotary axle, which in turn has limited the ability to use the axle's bore for auxiliary conduit and control lines. More and more, coiled tubing applications are increasing the numbers and capabilities of auxiliary conduit and control lines down the coiled tubing or as part of a multiline coiled tubing, such as encapsulated coiled tubing or concentric coiled tubing.

Accordingly, and herein, the reel axle 204 has a bore that is free of duties, other than rotational support, and thus the through bore can be made larger in diameter than that of prior art reels. The larger through bore is ideal for accommodating the working end of large diameter encapsulated coiled tubing and enabling use of fluid and electrical controls while running CT 2. Multiline connections at the axis A, extending from the axle bore and that rotate with the reel, are connected through a multiline swivel for on-the-go communication with any downhole tools and bottom hole assemblies.

Having reference to FIGS. 9 and 13, the CTRU 10 is self-propelled. However, as the reel 4 is inset in frame 200 of the CTRU 10, and the diametral extent being maximized, the reel 4 sits so low therein it nearly reaches the road clearance RC. Thus, the reel 4 can act as a power-transmission barrier between the back and front of the frame 200. Hence, a conventional drive shaft between a front power plant and a rear drive is impractical. Accordingly, a rear power plant 250 or pusher is provided and driveably connected to rear drive wheels 252. The power plant 250 is connected through a drop box or transfer case (not shown) for providing multiple outputs including a drive for the rear wheels 252, and various drives for hydraulics and other auxiliary equipment.

Hydraulics can be routed to the front of the carrier for hydraulic front wheel drive as applicable.

Having reference to FIG. 1A and FIG. 1B, in usual operations, an umbilical (not shown) enables connection to the injector unit 12 and operation of the CTRU 10 reel 14 from the injector unit's control cab 74.

The use of the separate CTRU 10 enables use of "plug-and-play" replacement of spent reels, or adapting for reloading with a reel of coiled tubing on a spooling jig brought on site. Separate reel controls on the CTRU 10 enable reloading using the spooling jig without involvement of the injector unit 12.

The embodiments of the invention for which an exclusive property or privilege is claimed are as follows:

1. A system for conveying coiled tubing (CT) into and out of a wellbore comprising:

- a first mobile unit having
- a first mobile frame having a drive end, a back end and a mast supported on the back end adjacent the wellbore, the mast pivotable between a transport position and an erect position;
- a CT injector moveable along the mast;
- a gooseneck; and
- a rotatable support between the gooseneck and the injector; and
- a second mobile unit having
- a second mobile frame having a CT reel and a reel drive, wherein

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when the second mobile unit is located at the drive end of the first mobile unit, the gooseneck is rotatable on the rotating support to the drive end to receive CT therefrom; and

when the second mobile unit is located at the back end of the first mobile unit, the gooseneck is rotatable on the rotating support to the back end to receive CT therefrom; and

the system further comprising a carriage for supporting the CT injector, and wherein

the mast further comprises a pair of parallel mast posts connected at the back end and at a crown;

the carriage being supported between the mast posts for moving the injector along the mast; and

wherein the gooseneck further comprises:

a proximal segment connected to the rotatable support, and

a distal segment connected to the proximal segment and pivotable between an extended position for forming an arcuate CT guide, and a folded position; and

when the gooseneck is in the folded position, the folded gooseneck has an effective turning radius that enables rotation between the drive end and back end; and

wherein the gooseneck further comprises: an actuator operative between the proximal and distal segments for manipulating the gooseneck between the extended and folded positions; and

wherein, at least when the gooseneck is in the folded position, the proximal segment is pivotable at a guide pivot at the rotating support for moving the effective turning radius of the folded gooseneck clear of the mast posts.

2. The system of claim 1 wherein the gooseneck further comprises a fold lock between the proximal and distal segments for retaining the gooseneck in the folded position.

3. The system of claim 2 wherein:

the carriage further comprises an injector frame supporting the CT injector, the frame being movable away from and towards the mast, and

wherein the effective turning radius of the folded gooseneck is clear of the mast posts.

4. A system for conveying coiled tubing (CT) into and out of a wellbore comprising:

a first mobile unit having

a first mobile frame having a drive end, a back end and a mast supported on the back end adjacent the wellbore, the mast pivotable between a transport position and an erect position;

a CT injector moveable along the mast;

a gooseneck; and

a rotatable support between the gooseneck and the injector; and

a second mobile unit having

a second mobile frame having a CT reel and a reel drive, wherein

when the second mobile unit is located at the drive end of the first mobile unit, the gooseneck is rotatable on the rotating support to the drive end to receive CT therefrom; and

when the second mobile unit is located at the back end of the first mobile unit, the gooseneck is rotatable on the rotating support to the back end to receive CT therefrom; and

the system further comprising a carriage for supporting the CT injector, and wherein the mast further comprises a pair of parallel mast posts connected at the back end and at a crown;

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the carriage being supported between the mast posts for moving the injector along the mast; and wherein the mast is extendible and wherein: each mast post further comprising:  
 a first mast section pivotally connected to the back end; 5  
 a second mast section, and  
 an extension pivot, pivotally connecting the second mast section to the first mast section; and  
 the crown connecting the second mast sections of each mast post; and further comprising a releasable lock 10  
 between each of the first and second mast sections, the releasable lock further comprising:  
 a latch pin connected to either the first or second mast section;  
 a lock claw pivotally actuated from the second or first 15  
 mast section respectively and wherein when the mast is in the erect position, the lock claw is actuated to engage the latch pin for locking the first and second mast sections together.

5. A folding mast for a coiled tubing (CT) injector, the folding mast supported from a frame, comprising:  
 a pair of parallel mast posts;  
 a carriage supported between the mast posts and adapted for moving the CT injector along the mast, 20  
 each mast post further comprising:  
 a first mast section for support from the frame, 25  
 a second mast section, and  
 an extension pivot, pivotally connecting the second mast section to the first mast section; and  
 a crown connecting the second mast sections of each mast 30  
 post; and  
 further comprising a releasable lock between each of the first and second mast sections, each releasable lock further comprising:  
 a latch pin connected to either the first or second mast 35  
 section;  
 a lock claw pivotally actuated from the second or first mast section respectively and wherein when the mast is in the erect position, the lock claw is actuated to engage the latch pin for locking the first and second mast 40  
 sections together.

6. A folding mast for a coiled tubing (CT) injector, the folding mast supported from a frame, comprising:  
 a pair of parallel mast posts;  
 a carriage supported between the mast posts and adapted 45  
 for moving the CT injector along the mast,  
 each mast post further comprising:  
 a first mast section for support from the frame,  
 a second mast section, and  
 an extension pivot, pivotally connecting the second mast 50  
 section to the first mast section; and

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a crown connecting the second mast sections of each mast post; and wherein each extension pivot further comprises:  
 a generally triangular fulcrum having a three apexes, a first apex co-axial with the extension pivot;  
 a first actuator extending between the first mast section and a second apex, and  
 a second actuator extending between the second mast section and a third apex, wherein  
 when the first actuator is actuated to retract, the second mast section is caused to rotate about the extension pivot; and  
 when the second actuator is actuated to retract, the second mast section is caused to further rotate about the extension pivot until the mast is in the extended position.

7. A rotating gooseneck for a coiled tubing (CT) injector supported on a wellbore side of a mast, comprising:  
 a rotatable support between the gooseneck and the CT injector;  
 a proximal segment of the gooseneck connected to the rotatable support, and  
 a distal segment connected to the proximal segment and pivotable between an extended position for forming an arcuate CT guide, and a folded position; and wherein 25  
 when the gooseneck is in the folded position, the folded gooseneck has an effective turning radius that enables rotation clear of the mast; and  
 wherein, at least when the gooseneck is in the folded position:  
 the proximal segment is pivotable at the rotating support for moving the effective turning radius of the folded gooseneck clear of the mast.

8. A rotating gooseneck for a coiled tubing (CT) injector supported on a wellbore side of a mast, comprising:  
 a rotatable support between the gooseneck and the CT injector;  
 a proximal segment of the gooseneck connected to the rotatable support, and  
 a distal segment connected to the proximal segment and pivotable between an extended position for forming an arcuate CT guide, and a folded position; and wherein 35  
 when the gooseneck is in the folded position, the folded gooseneck has an effective turning radius that enables rotation clear of the mast; and  
 further comprising a fold lock between the proximal and distal segments for retaining the gooseneck in the folded position.

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